Abstract—Friction Stir Welding (FSW) is an innovative manufacturing process, which is used to join two pieces of metal with frictional heating and plastic deformation due to stirring action. Melting is avoided during the process, therefore problems related to microstructure phase transformation (i.e., cooling from the liquid phase) are avoided. The temperature distribution in the weld zone, as a function of the heat generation, highly affects the evolution of the residual stresses in the work piece, hence the performance of the final product. Therefore, thermal models play a crucial role in detailed analysis and improvement of this process. In this study, a previously developed and validated three-dimensional steady state thermal model of FS welding of AA2024-T3 plates has been used for evaluating the quality of the candidate solutions. It should be noted that this is a computationally expensive model and closed form formulations (i.e. analytical equations) for the underlying physics are not available, which forces us to use them sparingly during the optimization procedure. A mathematical correlation model, a surrogate in other words, is iteratively constructed to replace the FSW simulations and guide the search towards feasible and promising regions. A new surrogate-based optimization algorithm named EICTS, Expected Improvement with Constrained Tournament Selection has been developed. The striking difference of EICTS from other surrogate based constrained optimization methodologies that it needs to construct only two surrogates, i.e. one for the objective function and another one to handle all constraint functions (i.e., instead of approximating each of them individually). EICTS is first tested on some well-known engineering problems with multiple constraints and finally on the FSW problem briefly mentioned above. Its runtime and convergence performances are compared with EIPF (Expected Improvement with Probability of Feasibility) method and found very promising.

I. INTRODUCTION

The friction stir welding (FSW) process is getting more attractive especially in aerospace and automotive industries where there is a high demand for lightweight structures built of materials having high strength-to-weight ratio such as aluminum alloys [1], [2]. First and foremost, the mechanical properties of the metal are preserved as much as possible since there is no melting during the process. It is also advantageous in case of welding large structures which cannot be heat-treated afterwards. The process starts with clamping the workpieces on to an anvil to avoid abutting surfaces spread apart. Then a rotating wear-resistant tool is submerged and traversed along the joint line while stirring the two pieces of metal together. The frictional heating, together with the plastic work provided by the forging and stirring motions, softens the material and makes the FSW tool move forward easier. The process is finalized by removing the tool out of the two workpieces and by letting it cool down to form the weld. These steps have been schematically shown in Fig. 1.

Since the development of the process in 1991, FSW modeling studies involving several research areas such as heat transfer [3], [4], [5], [6], material flow [7], material science and metallurgy [8], and solid mechanics [3], [4], [9], [10], [11] are increasing every year. However, the common ground behind those models is the requirement for high demanding computation time. Therefore, the number of numerical optimization studies is limited [12], [13], and design improvements mostly were performed by experimental works. Most of these numerical optimization studies are based on pure thermal models concerning single objectives or serving for inverse modeling purposes. The reason why the emphasis is put on thermal models is not only the less requirement for the computational resources, but also the dominant relationship between the microstructure as well as the residual stress evolution in the weld zone and the final the performance of the weld. Therefore, thermal models play a crucial role in detailed analysis and improvement of this process. Few multiobjective optimization studies regarding thermal [14], [15] and thermo-mechanical aspects (i.e., residual stresses) of the FSW process have recently been presented by [16].

Having given an overview about the general activities and challenges about the multi-physics simulation and optimization of the FSW process [12], [13], it is worth here to mention about the computationally more efficient optimization algo-
arithms which are based on approximating methods (surrogates, meta-models, or response surfaces in mathematical parlance [17], [18], [19], [20], [21], [22], [23], [24]). Most known surrogates in the literature vary from simple polynomial regression models and moving least squares to neural networks, radial basis functions, Kriging, and support vector regression. Some of these methods are also listed under machine learning, statistical learning, or in general supervised learning techniques. Despite the variety in their mathematical construction, they all work on the same consecutive principles: training (learning) and testing (prediction or generalization). Training, in simple terms, is the procedure of learning the behavior of the underlying response as a function of some chosen parameters, which can also be called as the mathematical mapping. Once this mapping is learned using limited sample size, e.g., in case of using multidisciplinary manufacturing process simulations, it can be used to iteratively replace the computationally expensive black-box function. This simpler model allows the user to predict any response at an unknown design set at a negligible cost.

This article is structured as follows. First, a three-dimensional steady state thermal model of FSW of AA2024-T3 plates simulated in COMSOL has been presented in section II. Next, a brief introduction to Kriging, i.e., the surrogate (approximation function), to be used in the Efficient Global Optimization (EGO) (see (section III-B)) is described in section III-A. Then two update criteria, EIPF and the proposed method EICTS, are introduced in sections III-C and III-D respectively. The results of the validation cases as well as the simulation-based optimization problem in FSW are given in section IV. Following the discussions of the results, the article is finalized with the concluding remarks and addressing the future work.

II. SIMULATION OF FSW

In this study, the temperature distribution during FSW of two AA2024-T3 plates has been simulated using commercial multi-physics finite element software COMSOL [25]. The plunge, the dwell, and the pull-out periods have been neglected; therefore, only the steady-state period has been the focus of the modeling procedure. This assumption alleviates some remarkable complexities and still allows capturing the first-order effects the process parameters on the fully developed temperature field in the welding domain [5], [6]. Moreover, the performance of the numerical optimization is enhanced by reducing the computational cost of the model, hence increasing the number of function evaluations in a limited time frame [14], [12].

The heat generation in FSW is often simulated by the application of a surface heat flux in case of sliding or a volume heat flux in case of sticking boundary condition [5], [6]. However, the uncertainty in the contact status at the interface reveals other problems related to the model input parameters such as the friction coefficient or the yield shear strength. In most of the studies, common effort is put into deriving the total heat generation or the friction coefficient from the tool force and torque measurements as the main heat source. However, this is conflicting with the aim of the thermal model that is in essence used to predict the heat generation. Besides, the need for the measurements for each different case having different process parameters would not be straightforward. In order to overcome these limitations, thermal models should be integrated with mechanical and flow models in which contact condition, deformation, etc. can be captured simultaneously. On the other hand, taking all these effects into account would obviously be an overkill for an optimization study since even only one function evaluation would take several days or weeks to compute [12].

In the present optimization study, a three-dimensional steady-state Eulerian thermal model involving an analytical heat source called Thermal-Pseudo-Mechanical (TPM) model [6], which is capable of incorporating with the prescribed material flow [5], has been implemented in COMSOL. It is a well-known phenomenon that once the material is heated, its yield stress decreases and vice versa. When the temperature exceeds the solidus temperature, it behaves as a fluid having almost no resistance to deformation; therefore, contribution to heat generation becomes negligible. Therefore, the solidus temperature acts as a switch button for turning the heat generation from "on" to "off". This information has been implemented here in the TPM model. As evident from its name, it is a purely thermal model which takes some mechanical information (i.e., yield strength variation of the metal with temperature) into account, thus bypassing the solution of the mechanical field. Even though some nonlinearity is introduced by application of this solution (i.e., temperature) dependent heat source, the computation time is still much more reasonable as compared to the solution time of a full thermo-mechanical model. The details of the model, i.e., heat source, boundary conditions, enmeshment, etc., are given in the following paragraphs.

For the purpose of predicting the thermal field in the work-piece, the classical time-dependent heat conduction equation should be solved regardless of the complexity of the heat source, see Eq. 1,

$$\rho c_p \dot{T} = \nabla(k \nabla T) + q_{vol},$$

where $\rho$ (kg/m$^3$) shows the material density, $c_p$ (J/kgK) the specific heat capacity, $T$ (K) the temperature output, $k$ (J/mK) the conductivity, and $q_{vol}$ (W/m$^3$) the volumetric heat source term. In case of describing the heat flow in a Eulerian reference frame under steady-state conditions, the time dependent term is removed and a convective term is added to Eq. 1 as given by the following equation,

$$0 = \nabla(k \nabla T) + q_{vol} - \rho c_p u \dot{T},$$

where $u$ is the velocity field vector defined analytically in the shear layer region (around the tool) which changes between the tool welding velocity and the tool rotational speed [5]. The heat generation ($q_{vol}$) defined in the shear layer regions is varying with the rotational speed ($\omega$), the position ($r(x, y)$),
TABLE I

<table>
<thead>
<tr>
<th>T [°C]</th>
<th>k [W/mK]</th>
<th>ρ [kg/m³]</th>
<th>cₚ [J/kgK]</th>
<th>σᵧ [MPa]</th>
</tr>
</thead>
<tbody>
<tr>
<td>20</td>
<td>100</td>
<td>2780</td>
<td>929</td>
<td>969</td>
</tr>
<tr>
<td>100</td>
<td>121</td>
<td>2767</td>
<td>969</td>
<td>261</td>
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<td>200</td>
<td>136</td>
<td>2749</td>
<td>1022</td>
<td>348</td>
</tr>
<tr>
<td>300</td>
<td>137</td>
<td>2729</td>
<td>1075</td>
<td>52</td>
</tr>
<tr>
<td>400</td>
<td>124</td>
<td>2709</td>
<td>1128</td>
<td>13</td>
</tr>
<tr>
<td>500</td>
<td>98</td>
<td>2689</td>
<td>1181</td>
<td>5</td>
</tr>
</tbody>
</table>

The yield strength of AA2024-T3 (σₘₚ)(T), and the shear layer thicknesses (tₛₛ𝐿), see Eq. 3:

\[ q_{vol}(x, y, T) = \frac{\omega r(x, y)\sigma_{yield}(T)}{\sqrt{3t_{SL}}} \] (3)

where \(u\) and \(v\) are dependent interpolation coefficient in a shear layer region, i.e.,

\[ u = -y\omega(1 - \zeta) + \zeta u_{weld}, \]
\[ v = x\omega(1 - \zeta), \] (4)

where \(u_{weld}\) is the tool feed rate and \(\zeta\) is the position dependent enmeshment coefficient in a shear layer region, i.e.,

\[ \zeta_{Sh-side}(z) = \frac{t_{plate} - z}{t_{plate} - t_{Sh-side-SL}}, \]
\[ \zeta_{Pr-side}(r) = \frac{t_{weld} - r}{t_{weld} - t_{Pr-side-SL}}, \]
\[ \zeta_{Pr-tip}(z) = \frac{z - z_{Pr-tip}}{t_{Pr-tip} - z_{Pr-tip}} \] (5)

where \(t_{plate}\), \(t_{Sh-side-SL}\), \(t_{Pr-side-SL}\), and \(t_{Pr-tip-SL}\) are, respectively, the thicknesses of the plate, the shoulder side, the probe side as well as the probe tip shear layers, and \(z_{Pr-tip}\) is the vertical coordinate of the probe tip.

Fig. 2 represents a characteristic temperature distribution in an FSW application with the appropriate thermal boundary conditions. The front surface of the plate is kept constant at the room temperature (20 °C). The convection heat flow is applied at the back surface of the workpiece. Thermal insulation is enforced on both sides of the plate. Asymmetric temperature distribution (i.e., higher temperature values are observed at the advancing side over the retreating side) caused by the material flow close to the tool shoulder is also captured as very well known [2], [27]. The anvil and the FSW tool are neglected in this model. This is due to two reasons: first, inclusion of these will introduce extra uncertainties in the model (temperature boundary condition at the tool holder head, the heat flux diffused into the tool, etc.), and second, the size of the enmeshment will get larger, and this will immensely increase the computation time. The steel backing plate is equivalently replaced by a heat flux boundary condition having a heat transfer coefficient (HTC) of 1000 W/m²K [27]. The cooling from the top surface is also taken into account by applying an HTC value of 10 W/m²K.

III. OPTIMIZATION

A. Surrogate Model: Kriging

Kriging is a well-known surrogate technique that is frequently used to approximate computationally expensive functions in the course of optimization. The method, named after a South African geologist D. Krige [28], was developed to estimate mineral concentrations within a particular field and popularized by the work of Sacks et al. [29], which made it also known as Design and Analysis of Computer Experiments. The procedure starts with obtaining a sample data of limited size (i.e., \(n\)-design sets each having \(d\)-variables), \(X_{n\times d} = [x^{(0)}, x^{(1)}, ..., x^{(n)}]^T\), and a corresponding vector of scalar responses \(Y_{n\times 1} = [y^{(1)}, y^{(2)}, ..., y^{(n)}]^T\). It is assumed that if design points, e.g., \(x^{(i)}\) and \(x^{(j)}\), are positioned close together in the design space, their respective function values \(y^{(i)}\) and \(y^{(j)}\) are expected to be similar, and vice versa. This can be formulated statistically by considering the correlation between two points as,
where \( \theta_k \) is a correlation parameter or hyperparameter (i.e., \( \theta_k = \theta_1, \theta_2, \ldots, \theta_d \)) which controls how fast the correlation changes from one point to the other one along each dimension. Here, Gaussian basis function is used; therefore the exponent is fixed at 2 yielding a smooth and continuous transition at \( x^{(i)} \).

Eq. 6 is used to build the symmetric correlation matrix \( (R) \) of all \( n \) points in \( X \), which will be used in the process of tuning the unknown hyperparameter \( \theta_k \) to maximize the likelihood of the assumed Gaussian model on the given dataset. Having the Kriging model parameters tuned, the next step is to predict a new response value, i.e., an objective or a constraint function value, at an unobserved design point using the sample data that are used to train the Kriging model. Ordinary Kriging predictor \( \hat{y}(\mathbf{x}) \) has such a form,

\[
\hat{y}(\mathbf{x}) = \hat{\mu} + r(\mathbf{x}, \mathbf{x}) \mathbf{R}^{-1} (y(\mathbf{x}) - 1\hat{\mu}),
\]

where \( r(\mathbf{x}, \mathbf{x}) \) is the linear vector of correlations between the unknown point to be predicted (\( \mathbf{x}^* \)) and the known sample points (\( \mathbf{x} \)), \( (\hat{\mu}) \) is the estimated mean, and \( 1 \) is an unit vector of size \( n \times 1 \). Ordinary Kriging assumes a constant term \( (\hat{\mu}) \) for the global fitting term in the predictor equation, whereas the Universal Kriging uses a known functional form. The second part on the right side of Eq. 7 represents the local deviation from the global term. Kriging is in general known for its good performance in fitting complex functional behavior; however, what makes Kriging a very popular surrogate technique is in essence its ability to estimate the mean squared error (MSE) at the unknown point,

\[
\hat{s}^2(\mathbf{x}^*) = \sigma^2 \left[ 1 - r^T \mathbf{R}^{-1} r + \frac{1 - 1^T \mathbf{R}^{-1} 1}{1^T \mathbf{R}^{-1} 1} \right],
\]

where \( \hat{s}^2 \) represents the MSE estimate. The third term inside the square parentheses is very small and is often neglected. Since Kriging is an interpolation method, \( \hat{s}^2 \) reduces to zero at the sample points and consequently \( \hat{y} \) becomes equal to the corresponding response value.

\[ I(x) = \max (y_{best} - Y(x)) \]
TABLE II
A SAMPLE OF 8 SOLUTIONS WITH THEIR OBJECTIVE (Yi) VALUE AND CONSTRAINT VIOLATION (CV1−3)
VALUES

<table>
<thead>
<tr>
<th>Xi</th>
<th>Yi</th>
<th>CV1</th>
<th>CV2</th>
<th>CV3</th>
</tr>
</thead>
<tbody>
<tr>
<td>X1</td>
<td>3628.2</td>
<td>0.10786</td>
<td></td>
<td></td>
</tr>
<tr>
<td>X2</td>
<td>2144.4</td>
<td>-0.72429</td>
<td>0.038429</td>
<td>15.129</td>
</tr>
<tr>
<td>X3</td>
<td>39.876</td>
<td>-0.02</td>
<td>0.3628</td>
<td>4323.5</td>
</tr>
<tr>
<td>X4</td>
<td>151.34</td>
<td>0.12786</td>
<td>0.061571</td>
<td>14.042</td>
</tr>
<tr>
<td>X5</td>
<td>172.75</td>
<td>-0.005</td>
<td>-0.21757</td>
<td>14.048</td>
</tr>
<tr>
<td>X6</td>
<td>2332.8</td>
<td>-0.82714</td>
<td>-0.38071</td>
<td>12.944</td>
</tr>
<tr>
<td>X7</td>
<td>3360.3</td>
<td>-0.025</td>
<td>-0.34071</td>
<td>12.944</td>
</tr>
<tr>
<td>X8</td>
<td>4323.5</td>
<td>-0.02</td>
<td>-0.72743</td>
<td>15.276</td>
</tr>
</tbody>
</table>

D. Proposed Method: EICTS

In this paper, a new constraint handling methodology is proposed within the EGO framework without transforming the constrained problem into an unconstrained one. As usual, a uniform sampling method such as optimal Latin Hyper-Cube Sampling (LHS) method is applied to obtain the initial sampling set within the bounded design space. Next, the true objective and constraint function values (i.e. high-fidelity simulations) are computed at these initial design sites. Up to this point, it is same with the standard EGO (both with $E[I(x)]$ and EIPF criterions) algorithm. The proposed method needs to build only two surrogates; one for the objective function and another one for the total constraint violation ($TCV_i$), which is computed using all constraint violations. The constraints are defined in a way that negative values indicate that the solution is feasible whereas the positive value indicates that the solution is infeasible. While computing the $TCV$ value, only positive values (i.e. CVi values of those infeasible solutions) are taken into account. However, building only one surrogate for multiple surrogates having values at different orders of magnitude requires an additional normalizing step. To make the following discussion more clear, a sample of 8 solutions having an objective ($Y_i$) and three constraint violation values ($CV_i^{1−3}$) is provided in Table II.

In the next step, each $CV_i$ column is checked separately: feasible solutions ($CV_i \leq 0$) are normalized between -1.0 and 0.0, infeasible solutions ($CV_i > 0$) are normalized between $-10^{-8}$ and 1.0. Then, in order to compute single $TCV_i$ value for each $X_i$ solution, rows having only positive or only negative values are summed up, however in other rows, only positive values are summed up. The normalized $CV_i$ and the computed $TCV_i$ values are shown in Table III.

According to Table III solutions $X_1, X_5, X_4, X_5, X_8$ are infeasible and the other 3 solutions are feasible. These $TCV_i$ values are then approximated using Kriging function. The next important step is to compute the standard $E[I(x)]$ values for all candidate solutions in the course of global search algorithm. The purpose is to find feasible candidate solutions (i.e., $TCV_i \leq 0$) with maximum $E[I(x)]$ values. To efficiently search the constrained design space Constrained Tournament Selection, with tournament size equal to 5, is implemented. During the iterations of the global optimization algorithm, 5 randomly selected individuals are first compared with respect to their $TCV_i$ values: i) if all (or at least one) $TCV_i$ values are negative (i.e., feasible) then the solution with the maximum $E[I(x)]$ value wins the tournament, ii) if all $TCV_i$ values are positive (i.e., infeasible) then the solution with the minimum $TCV_i$ value wins the tournament. At the end of the global optimization procedure, the optimal candidate solution, which is found using the surrogate models, is re-evaluated using high-fidelity simulations.

IV. RESULTS

In the following sections, three well known analytical engineering constrained optimization problems are given to validate the performance of the proposed method, EICTS. For each test problem, 30 experiments with different initial LHS set are performed. These three problems, Gas Transmission Compressor Design (GTC), Pressure Vessel Design (PVD), Welded Beam (WB), are well studied by the constrained optimization researchers, however the application of surrogate-based constrained optimization algorithms are limited. Moreover, the performance of EICTS is only compared with EIPF due to the limited availability of the alternative open-source algorithms. Our main objective was to achieve comparable results in shorter computational time. The summary of the results in Table IV as well as in Figs. 4, 5, 6 and 7 show that even better solutions (i.e., better feasible objective values as well as closer solutions to the analytical optimum solution) are obtained in shorter time period.

A. Validation Cases

In the following three engineering problems, the global optimum solutions are known and reported in the literature. 30 experiments are performed for each validation case using both EIPF and EICTS methods. All problems have four design variables. The initial sample sets include 20 solutions and a budget of 40 infill point calculations are allowed for each experiment. Normalized distance of the current best solution to the analytical optimum solution and the 95% confidence intervals are shown in the following figures. Since algorithms are tested with the same initial sample sets, the average best and variance values between 1st and 20th samples are same. The infill points start to deviate from each other due to different algorithm performances.
1) Gas Transmission Compressor Design (GTCD): The problem is taken from [35]. It has 4 design variables and 1 constraint function. It is clearly seen from Fig. 4 that EICTS is able to find better solutions (i.e., closer to optimal solution) in approximately 10 out of 30 experiments.

2) Pressure Vessel Design (PVD): The problem is taken from [36] and [37]. It has 4 design variables and 3 constraint functions. In this case, the performances look closer but EICTS still performs better. The runtime performance of the two algorithms are also given in Table IV and EICTS starts to get faster as compared to EIPF, because different surrogate approximations for the multiple constraint functions need to be performed by EIPF, whereas only single surrogate approximation for all the constraint functions is needed for EICTS.

3) Welded Beam (WB): The last validation problem is taken from [36], [37], [38]. It has 4 design variables and 6 constraints. The performances in Fig. 6 look similar however the runtime performance of EICTS is approximately 3.5 times faster than EIPF. Moreover, Table IV shows the average number of feasible solutions found in 30 experiments for each problem and EIPF could not find any feasible solution, whereas EICTS could find at least 1 or 2 feasible solutions in approximately 10 out of 30 experiments.

B. Simulation-based Optimization Problem: FSW

Original problem was formulated as a multi-objective optimization problem in [15] and here it is converted to a single-objective optimization problem. The design variables are the radius of the tool shoulder \( (8 \leq R_{sh} \leq 12 \text{ mm}) \), radius of the probe \( (3 \leq R_{pr} \leq 6 \text{ mm}) \), welding speed \( (1 \leq u_{weld} \leq 8 \text{ mm/s}) \) and the tool rotational speed in terms of revolutions per minute \( (400 \leq n_{rev} \leq 1000 \text{ rpm}) \). As common in other manufacturing processes as well, the production rate is desired to be maximized in the FSW process; this can obviously be achieved by increasing the traversing speed \( (u_{weld}) \); however, increasing the welding speed promotes the risk of tool probe failure due to colder (i.e., harder) material ahead of tool. Therefore, temperature gradient in the narrow region of the tool probe surface (i.e., 1 mm ahead and one fourth of the height) should also be minimized for safety purposes. This evaluation can be done in more detail with a computational solid mechanics (CSM) or a computational fluid mechanics (CFD) approach; however, the computational cost would be very high (varies from hours to a day), and consequently, the integration of these type of models with the numerical optimization algorithms would be impractical. Hence, this safety issue has been considered as the objective function (i.e., to minimize), and thus bypassed the costly CSM/CFD calculations using a pseudo-mechanical link with an engineering intuition. Some of the other important constants in the FSW simulation are the thickness of the plate \( (7 \text{ mm}) \), the height of the tool probe \( (6 \text{ mm}) \), observed shear layer thickness at the shoulder and probe sides as well as at the tip of the probe are \( 2 \text{ mm}, 0.5 \text{ mm} \) and \( 0.25 \text{ mm} \), respectively. The welded plates are 100 mm-long and 50 mm-wide. Three constraints are defined: 1 and 2) Average temperature in the
shoulder side shear layer should be between 450°C and 500°C respectively, 3) the material temperature in front of the tool probe should be higher than 425°C.

The optimal solution to this FSW problem is \([R_{shoulder}^*, R_{probe}^*, u_{weld}^*, n_{rev}^*] = [12 \text{ mm}, 3 \text{ mm}, 1 \text{ mm/s}, 700 \text{ rpm}]\). This is also intuitive because promoting a large volume of heat generation by using a FSW tool having the maximum tool shoulder radius and minimum tool probe radius (i.e., Volume\(_{sh-\text{side}-SL} = \pi(R_{shoulder}^2 - R_{probe}^2)l_{sh-\text{side}-SL}\)) as well as keeping the traversing speed at its minimum value leaves only one process parameter to optimize, i.e., that is \(n_{rev}^*\). Due to higher computational cost of the simulations, 10 experiments are performed instead of 30 only for this problem. The results are shown in Fig. 7 and it clearly shows the dominance of the EICTS results. EICTS clearly finds process and design parameters yielding lower temperature difference between the probe and the incoming material. Moreover, the variance in the average of best solutions in 10 experiments are much narrower which shows the reliability of the proposed method. The runtime performance (~1.5 times faster) also supports the success of EICTS.

![Fig. 7. Average of the smallest Euclidean distance to the optimal solution in 30 experiments for the FSW problem.](image)

### TABLE IV
PERFORMANCE COMPARISON OF EIPF AND EICTS, WITH RESPECT TO (1) AVERAGE NUMBER OF FEASIBLE SOLUTIONS, (2) AVERAGE COMPUTING TIME AND (3) BEST FEASIBLE FITNESS VALUE AMONG 30 EXPERIMENTS.

<table>
<thead>
<tr>
<th>Performance Criterion</th>
<th>Problem</th>
<th>EIPF</th>
<th>EICTS</th>
</tr>
</thead>
<tbody>
<tr>
<td>(n_{feas,avg})</td>
<td>GTCD</td>
<td>41.46/20</td>
<td>20.30/20</td>
</tr>
<tr>
<td></td>
<td>PVD</td>
<td>0.366/0.366</td>
<td>1.266/0.366</td>
</tr>
<tr>
<td></td>
<td>WB</td>
<td>None</td>
<td>0.0335</td>
</tr>
<tr>
<td></td>
<td>FSW</td>
<td>15.30/15.30</td>
<td>6.758/6.758</td>
</tr>
<tr>
<td></td>
<td>GTCD</td>
<td>225.95/225.95</td>
<td>214.63/214.63</td>
</tr>
<tr>
<td></td>
<td>PVD</td>
<td>355.15/355.15</td>
<td>210.53/210.53</td>
</tr>
<tr>
<td></td>
<td>WB</td>
<td>702.25/702.25</td>
<td>213.50/213.50</td>
</tr>
<tr>
<td></td>
<td>FSW</td>
<td>5385.3/5385.3</td>
<td>3797.8/3797.8</td>
</tr>
<tr>
<td>(CPU-time_{avg})</td>
<td>GTCD</td>
<td>40.75/39.75</td>
<td>3.035/175.86</td>
</tr>
<tr>
<td></td>
<td>PVD</td>
<td>6680.9/6641.2</td>
<td>6641.2/6641.2</td>
</tr>
<tr>
<td></td>
<td>WB</td>
<td>None</td>
<td>5.195</td>
</tr>
<tr>
<td></td>
<td>FSW</td>
<td>3/2/2</td>
<td>5/2/2</td>
</tr>
</tbody>
</table>

### V. CONCLUSIONS

The steady-state thermal simulation of the Friction Stir Welding (FSW) process is implemented in COMSOL for optimizing the process parameters and the tool geometry to minimize the risk of tool failure (i.e., by minimizing the temperature gradient between the incoming material and tool probe). The average temperature is desired to be kept above 450°C to avoid tool pin failure and below 500°C to reduce the tool wear. The effect of the tool rotation on the distribution of the temperature field is also taken into account. Since the average computational time for a single FSW simulation is changing from 5 minutes to 9 minutes (on a desktop computer with Intel Core i7, 2.67 GHz CPU and 8 GB of RAM), these high fidelity simulations need to be executed sparingly. Therefore a surrogate-based optimization methodology, in which the computationally expensive function calls are replaced by low fidelity approximation functions (i.e., surrogates), is applied. A new constraint handling methodology, employing Constrained Tournament Selection, is developed and integrated within the well known efficient global optimization (EGO) framework. The runtime and convergence performance of the algorithm is tested on three analytical engineering test problems, and finally, on the simulation-based optimization problem in FSW. The performance of the proposed method, EICTS (Expected Improvement with Constrained Tournament Selection), is compared with EIPF (Expected Improvement with Probability of Feasibility). A budget of 60 high-fidelity simulations is allowed. Findings can be summarized as follows:

- Multiple number of constraint functions are approximated by only a single surrogate function, which is a different approach from most other surrogate-based optimization methods presented in the literature. This shortcut obviously speeds up the model building process.
- The order of magnitudes of any constraint can be handled with this method, because all constraint values are properly normalized without using any parameters (i.e., without knowing the maximum value of the constraint function can get, which is then used as a denominator constant). The proposed method does not need the actual constraint function violation values; instead it only compares the relative magnitudes of the total constraint violation (TCV) value within the Tournament Selection process to guide the search towards the feasible design region.
- EICTS has been tested on relatively difficult well known engineering test problems as well as the simulation based optimization problem for the FSW process. Both the runtime and convergence performances found to be very promising.

A few pointers to improve the performance of the proposed method could be given as following. Here, Kriging is used for both the objective and constraint functions, but the methodology can be extended to other surrogates (Support Vector Machines, Radial Basis Functions, etc.) as long as a measure of uncertainty (Mean Squared Error) estimation for the
objective function is available. Such information can also be incorporated while handling constraints, i.e., instead of using only $TCV_i$, the value of $TCV_i + \hat{s}_i^2$ can be evaluated ($\hat{s}_i^2$ is the estimation of MSE for $TCV_i$). In that case, predictions at crowded regions would result in lower $\hat{s}_i^2$ values, whereas predictions at less explored regions would result in higher $\hat{s}_i^2$ values. Handling higher number of design variables is an important aspect of the constrained optimization practice, and it should be noted that the Bayesian Optimization (BO) Algorithms (such as EGO) are known to perform slower at higher number of dimensions ($d \geq 15$). A trust-region-based BO methodology could be a good alternative for such a case. This will be addressed in a further study.

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