

# Tuning the Wall-Following Controller

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We would like to tune the parameters of the wall-following controller so that it is as close to critically-damped as possible. That is, it converges to the setpoint as quickly as possible without overshooting.

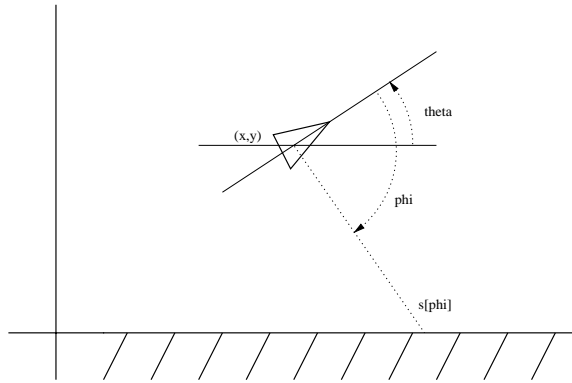


Figure 1: The robot is at position  $(x, y)$  and orientation  $\theta$ . The range sensor in direction  $\phi$  senses distance  $s_\phi$ , but in this paper we assume that  $y$  and  $\theta$  are sensed directly.

The dynamical model of the robot (Figure 1) is  $\mathbf{x}' = f(\mathbf{x}, \mathbf{u})$ , with constant forward velocity  $v$  and exogenously specified angular velocity  $\omega$ .

$$\mathbf{x}' = \begin{bmatrix} x' \\ y' \\ \theta' \\ v' \end{bmatrix} = \begin{bmatrix} v \cos \theta \\ v \sin \theta \\ \omega \\ 0 \end{bmatrix} \quad (1)$$

## The Wall-Following Controller

We use a slightly simplified version of the wall-following controller from [2].

The wall-following control law (3) sets angular velocity  $\omega$ , responding to positional error  $e = y - y_{set}$  and orientation error  $\theta$ , and assuming that forward velocity  $v$  is constant.

We want to specify the control law so that the behavior of the system will be described by

$$\ddot{e} + k_\theta \dot{e} + k_e e = 0. \quad (2)$$

where the constants  $k_e$  and  $k_\theta$  are tuned to make the system behave well (i.e., critically damped convergence  $e \rightarrow 0$ ).

For small values of  $\theta$ ,

$$\dot{e} = v \sin \theta \approx v\theta$$

and

$$\ddot{e} = v \cos \theta \dot{\theta} \approx v\omega,$$

so we can transform the general system description (2) into a control law: a rule for specifying the value of the controlled variable  $\omega$  as a function of the values of the observed variables  $e$ ,  $\theta$  and  $v$ :

$$\omega = \frac{1}{v}[-k_\theta v\theta - k_e e]. \quad (3)$$

## Qualitative Behavior

Any elementary discussion of differential equations and dynamical systems (e.g. [1]) provides the qualitative framework we need to tune this controller.

When obeying the wall-following control law, the robot's behavior approximates the linear harmonic oscillator, which is a special case of the general linear second-order system:

$$a\ddot{x} + b\dot{x} + cx = 0. \quad (4)$$

The behavior of this system is determined by the roots of its characteristic equation:

$$r_1, r_2 = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}.$$

The qualitative behavior  $x(t)$  is determined by the qualitative properties of the roots, which are determined in important part by the sign of the *discriminant*:

$$D = b^2 - 4ac.$$

- If the roots have non-zero imaginary part (i.e.,  $D < 0$ ), the behavior oscillates. If the roots are purely imaginary (i.e.,  $D < 0$  and  $b = 0$ ), the oscillation is periodic.
- If either root has a positive real part, the behavior diverges. In a usefully controlled system, the behavior must converge, so both roots must have negative real parts. If  $D < 0$ , we require only that  $b > 0$ . If  $D > 0$ , we also need to have  $b > \sqrt{b^2 - 4ac}$ , which therefore requires that

$$0 < c < \frac{b^2}{2a}.$$

- *Critical damping* occurs at the boundary between oscillatory and non-oscillatory behavior; that is, where  $D = 0$ , so:

$$c = \frac{b^2}{4a}. \tag{5}$$

## Tuning the Controller

To make the behavior of the system (2) critically damped, we apply (5) and require that

$$k_e = \frac{k_\theta^2}{4} \text{ or equivalently, } k_\theta = \sqrt{4k_e}. \tag{6}$$

## Experimental Results

The model `rwal12.m` implements this controller, with some modifications. In order to avoid divergence when  $v \approx 0$  during starting and stopping, the  $1/v$  term in (3) is replaced by  $\min(v^2, 1/\max(0.01, v))$ .

Setting  $k_e$  to values in the range  $[0.1, 0.6]$  controls how aggressively the controller seeks the setpoint. Setting  $k_\theta = \sqrt{4k_e}$  makes the resulting controller critically damped, as expected. High gains at lower velocities results in turns that might be overly aggressive.

## Next Steps

- Set the gain as a function of forward velocity, to see whether this gives better performance.

- What are the applicability conditions for this controller? How close is  $\theta \approx 0$ ? What happens if the robot is close to facing the wall?

## References

- [1] M. Hirsch and S. Smale. *Differential Equations, Dynamical Systems, and Linear Algebra*. Academic Press, New York, NY, 1974.
- [2] P. van Turenout, G. Honderd, and L. J. van Schelven. Wall-following control of a mobile robot. In *IEEE International Conference on Robotics and Automation*, pages 280–285, 1992.