

TWO-DIMENSIONAL DIGITAL FILTERING AND ITS  
UNCORRELATED ERROR ANALYSIS\*

by

Ming-Duenn Ni and J. K. Aggarwal  
Department of Electrical Engineering

Technical Report No. 175  
July 15, 1975

INFORMATION SYSTEMS RESEARCH LABORATORY

ELECTRONICS RESEARCH CENTER  
THE UNIVERSITY OF TEXAS AT AUSTIN  
Austin, Texas 78712

\*Research supported in part by the Joint Services Electronics Program under JSEP Contract F44620-71-C-0091 and by the National Science Foundation under Grant GK-42790.

Approved for public release; distribution unlimited.

## ABSTRACT

The concept of a two-dimensional recursive digital filter is introduced and block diagram representations are given. Error analyses for both floating-point and fixed-point two-dimensional digital filters are carried out. A systematic way of estimating the mean squared errors due to roundoff, coefficient and input quantizations is discussed. Norm error bounds are also derived. Simulations of the implementations of digital filters are discussed, and corresponding to these simulations error calculations are performed. Numerical examples are given. The derived analytic results are shown to be in good agreement with the simulation results.

## TABLE OF CONTENTS

	Page
ABSTRACT . . . . .	iii
TABLE OF CONTENTS . . . . .	v
LIST OF FIGURES . . . . .	vii
CHAPTER I - INTRODUCTION . . . . .	1
CHAPTER II - TWO-DIMENSIONAL DIGITAL FILTERS . . . . .	5
CHAPTER III - ERROR ANALYSIS FOR TWO-DIMENSIONAL DIGITAL FILTERS EMPLOYING FIXED-POINT ARITHMETIC . . . . .	12
CHAPTER IV - ERROR ANALYSIS FOR TWO-DIMENSIONAL DIGITAL FILTERS EMPLOYING FLOATING-POINT ARITHMETIC . . . . .	34
CHAPTER V - DISCUSSION AND CONCLUSION . . . . .	57
APPENDIX I . . . . .	59
APPENDIX II . . . . .	66
REFERENCES . . . . .	100

## LIST OF FIGURES

Figure	Title	Page
1	Block Diagram Representation for Director Filtering Process . . . . .	8
2	Block Diagram Representation for Canonic Filtering Process . . . . .	9
3	Flow Graph for Fixed-Point Direct Filtering Process . . . . .	14
4	Flow Graph for Fixed-Point Canonic Filtering Process . . . . .	15
5	Block Diagram Interpretations for Director Filtering Process . . . . .	19
6	Block Diagram Interpretations for Canonic Filtering Process . . . . .	20
7	$G(z_1, z_2) = \frac{1}{1 + ax_1^{-1} + bz_2^{-1} + cz_1^{-1} z_2^{-1}}$	24
8	Flow Diagram for Floating-Point Direct Filtering Process . . . . .	35

## I. INTRODUCTION

Digital filtering of two-dimensional digital data is needed in many applications. For example, the processing of seismic records, gravity and magnetic data, and scene analysis and picture processing require two-dimensional filtering. Prior to 1965, the implementation of the two-dimensional digital filtering processes mostly used the two-dimensional direct convolution algorithm which is characterized by the double sum:

$$w_{mn} = \sum_{j=0}^m \sum_{k=0}^n g_{jk} x_{m-j, n-k}$$

where  $\{x_{jk}\}$  is the input sequence, which, for example, is the digitized recorded image,  $\{g_{jk}\}$  is the "weight matrix", which corresponds to the impulse response in the one-dimensional case, and  $\{w_{jk}\}$  is the output sequence, which, for example, is the enhanced image. In this method the output,  $w_{mn}$ , is the weighted sum of all past values of the input sequence, i.e.  $\{x_{jk}\}$ ,  $0 \leq j \leq m$ , and  $0 \leq k \leq n$ . A variation of the direct convolution technique is the method where a partial set of the past values of the input sequence is used to obtain the output  $w_{mn}$ . Direct convolution has a serious drawback, its requirements of a large number of arithmetic operations (multiplications and additions). The FFT algorithm, discovered in 1965, can provide a great deal of reduction in the number of arithmetic operations, and is being widely used. The FFT makes filtering feasible by use of the frequency domain equation,

$$W(\omega_1, \omega_2) = G(\omega_1, \omega_2) X(\omega_1, \omega_2) ,$$

where  $W(\omega_1, \omega_2)$ ,  $G(\omega_1, \omega_2)$  and  $X(\omega_1, \omega_2)$  are discrete Fourier transforms

of the sequences  $\{w_{mn}\}$ ,  $\{g_{mn}\}$ , and  $\{x_{mn}\}$  respectively, which are assumed to be periodic, and  $\omega_1$  and  $\omega_2$  are the two spatial radian frequencies.

The recursive algorithm provides another technique for the implementation of the filtering processes, especially for very large amounts of data. It is already known that the recursive techniques are more powerful (in the sense that its computational and memory requirements are fewer) than the FFT algorithm in a large number of one-dimensional cases. Therefore, it is desirable to study the related problems in two-dimensional recursive filtering.

There are several reports discussing two-dimensional recursive digital filters ([1], [2], [3]). For example, Shanks, Treitel and Justice ([2]) formulate two-dimensional recursive filters by the two-dimensional Z-transform and linear difference equations. They also study the stability of the filters and extend synthesis methods in the one-dimensional case to the two-dimensional case. Huang ([3]) simplifies Shanks' stability theorems ([1]). Farmer and Gooden ([21]) describe some of the computational problems associated with the approximation of unstable recursive digital filters by stable recursive digital filters. Hall ([22]) compares the computation required for the three spatial frequency filtering techniques which are direct convolution, fast Fourier transform, and recursive filtering. Other reports which touch upon two-dimensional recursive filtering are ([23], [24], [25]).

Besides considering the stability and the synthesis problems ([1], [2], [3]), we must also consider the effects of finite word length in the design of two-dimensional recursive digital filters. As in one-dimensional digital filters, the effects of finite word length also lead to the following three sources of error; namely, (1) the quantizations of input signals and initial states, (2) the quantizations of the filter coefficients, and (3) the rounding off of arithmetic operations. These sources of error cause the actual outputs of the digital filters to be different from the ideal outputs.

It is important to know whether a certain accuracy can be achieved if the digital filters are simulated on general purpose computers where the word length is usually fixed, or to determine the minimum word length needed for a specific performance accuracy if the digital filters are constructed with digital hardware. The effects of the three sources of error and the methods of analyzing them generally depend on the types of arithmetic (e.g., fixed-point arithmetic, floating-point arithmetic, or block floating-point arithmetic). There are many reports on fixed-point one-dimensional digital filters. For example, Jackson ([16], [17]) analyzed roundoff noise for digital filters realized in various forms (i.e., direct, parallel, and cascade forms). Gold and Rader ([20]) studied the effects of parameter quantization on the poles of a digital filter. Jackson ([18]) and Ebert and etc. ([19]) investigated the limit cycle oscillations due to roundoff after multiplication and overflow at the adder. There are also some papers on floating-point one-dimensional digital filters. Sandberg ([4]) derived an absolute upper bound on the error accumulations due to roundoffs in arithmetic operations. Kaneko and Liu ([8], [9]) derived an expression for the mean squared error caused by roundoff error accumulations assuming that the input signal is zero mean and wide sense stationary. Kan and Aggarwal ([6]) studied the error properties of digital filters realized in canonical form. Oppenheim and Weinstein ([13], [14]) examined and tested the roundoff errors of first and second order digital filters with zeros at infinity and gave expressions of output error to signal ratios for white noise inputs. Generally, the methods (e.g., [4], [6], [8], [9], [13], [14] and etc.) and the expressions (e.g., [4], [6], [8], and etc.) for roundoff errors are quite readily extended to recursive digital filters. However, a fundamental difficulty of two-dimensional digital filters is that we generally cannot factorize a two-dimensional recursive digital filter into a multiplication of lower order digital filters. This fundamental difficulty has caused serious

problems in the designing and analyzing of two-dimensional recursive digital filters. For example, we can obtain integral results in closed form for the expressions given by Kaneko and Liu ([8], [9]), but when the expressions are extended to two dimensions we generally cannot get similar results, although numerical approximations are possible.

In this manuscript we review some basic definitions and consequences and give block diagram representations for two-dimensional digital filters. We formulate a systematic way of estimating the output mean squared errors and the output norm error bounds for output errors due to the effects of finite word length for both fixed-point and floating-point two-dimensional digital filters. We give several examples to demonstrate the validity of the method. We also have two appendices. Appendix I describes the properties of the two-dimensional Z-transform needed for the development of the present report. Appendix I also proves a lemma which is essential to the derivation of the output norm error bounds. Appendix II lists some of the programs used to obtain the numerical results. "Two-dimensional" will be designated by "2D" henceforth for brevity.

## II. 2D DIGITAL FILTERS

A one-dimensional recursive digital filter is described by the linear difference equation:

$$w_n = \sum_{k=0}^N b_k x_{n-k} - \sum_{k=1}^M a_k w_{n-k} \quad (1)$$

- where (i)  $n \geq 0$ ,  
 (ii)  $N < M$ ,  
 (iii)  $\{x_n\}$  is the input sequence, and  
 $x_i = 0$ , for  $i < 0$ ,  
 (iv)  $\{w_n\}$  is the output sequence, and  
 $w_j = W(j)$ ,  $j = -1, \dots, -M$   
 $= 0$ ,  $j < -M$ .

Programs for a general purpose digital computer may be written or special purpose hardware may be built for performing the computation of Eq. (1). Extending the algorithm of Eq. (1) to two dimensions, one gets the following 2D computational algorithm:

$$w_{mn} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} x_{m-j, n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} w_{m-j, n-k} \quad (2)$$

- where (i)  $m \geq 0$  and  $n \geq 0$ ,  
 (ii)  $M_b \cdot N_b \leq M_a \cdot N_a$ ,  
 (iii)  $\{x_{mn}\}$  is the input sequence, and  
 $x_{jk} = 0$ , for  $j < 0$  or  $k < 0$ ,

(iv)  $\{w_{mn}\}$  is the output sequence, and

$$\begin{aligned} w_{jk} &= W(j, k), \quad k = 0, -1, \dots, -N_a, \\ &\quad j = 0, -1, \dots, -M_a, \\ &\quad j + k \neq 0, \\ w_{jk} &= 0, \text{ for } k < -N_a \text{ or } j < -M_a. \end{aligned}$$

Equation (2) is a 2D linear difference equation and represents a 2D linear discrete system. When the input sequence  $\{x_{mn}\}$ , the output sequence  $\{w_{mn}\}$ , and the coefficients  $a$ 's and  $b$ 's are digital quantities, it is called a 2D digital filter. Further, if all of the  $a_{jk}$ 's ( $j+k \neq 0$ ) are zero, it is nonrecursive, otherwise it is recursive.

In Appendix I, the 2D Z-transform is defined and some of its salient properties are listed. Its use in 2D digital filters is discussed in the following. Taking the 2D Z-transform of the 2D linear difference Eq. (2), and assuming all initial conditions are zero, one gets

$$W(z_1, z_2) = G(z_1, z_2) \cdot X(z_1, z_2) \quad (3)$$

where

$$G(z_1, z_2) = \frac{N(z_1, z_2)}{D(z_1, z_2)} \quad (4)$$

$$\begin{aligned} &= \frac{\sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} z_1^{-j} z_2^{-k}}{\sum_{j=0}^{M_a} \sum_{k=0}^{N_a} a_{jk} z_1^{-j} z_2^{-k}}. \quad (5) \\ &= \frac{\sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} z_1^{-j} z_2^{-k}}{1 + \sum_{\substack{j=0 \\ j+k \neq 0}} \sum_{k=0}^{N_a} a_{jk} z_1^{-j} z_2^{-k}} \end{aligned}$$

$G(z_1, z_2)$  is called a 2D digital transfer function, and may be used to represent a 2D digital filter.

A 2D unit point function is the sequence  $\{x_{mn}\}$  such that

$$\begin{aligned} x_{mn} &= 1, \quad m = n = 0, \\ &= 0, \quad \text{otherwise}, \end{aligned}$$

and the response of a digital filter to such an input is called its "point spread response". If

$$G(z_1, z_2) = \sum_{j=0}^{\infty} \sum_{k=0}^{\infty} g_{jk} z_1^{-j} z_2^{-k}, \quad (6)$$

the point spread response is given by the 2D sequence

$$\{g_{jk}\}_{j=0}^{\infty} \quad {}_{k=0}^{\infty}, \quad (7)$$

furthermore, the response of the filter to the input sequence  $\{x_{mn}\}$  is given by

$$w_{mn} = \sum_{j=0}^m \sum_{k=0}^n x_{jk} g_{m-j, n-k} = \sum_{j=0}^m \sum_{k=0}^n x_{m-j, n-k} g_{jk}. \quad (8)$$

In the above Eqs. (6), (7), and (8), it is assumed that the digital filter is causal. The inversion formula and other techniques for obtaining point spread response (7) from the transfer function (5) are discussed in Appendix I.

The difference Eq. (2) can be represented by the block diagram as shown in Figure 1. The 2D Z-transform relationship is given by Eqs. (3), (4), and (5). There are many block diagrams with  $G(z_1, z_2)$  equivalent to that of Figure 1. Different block diagrams signify different implementations of  $G(z_1, z_2)$ , and lead to different error properties. Figure 2 is an example in which the block diagram is described by the following pair of equations,

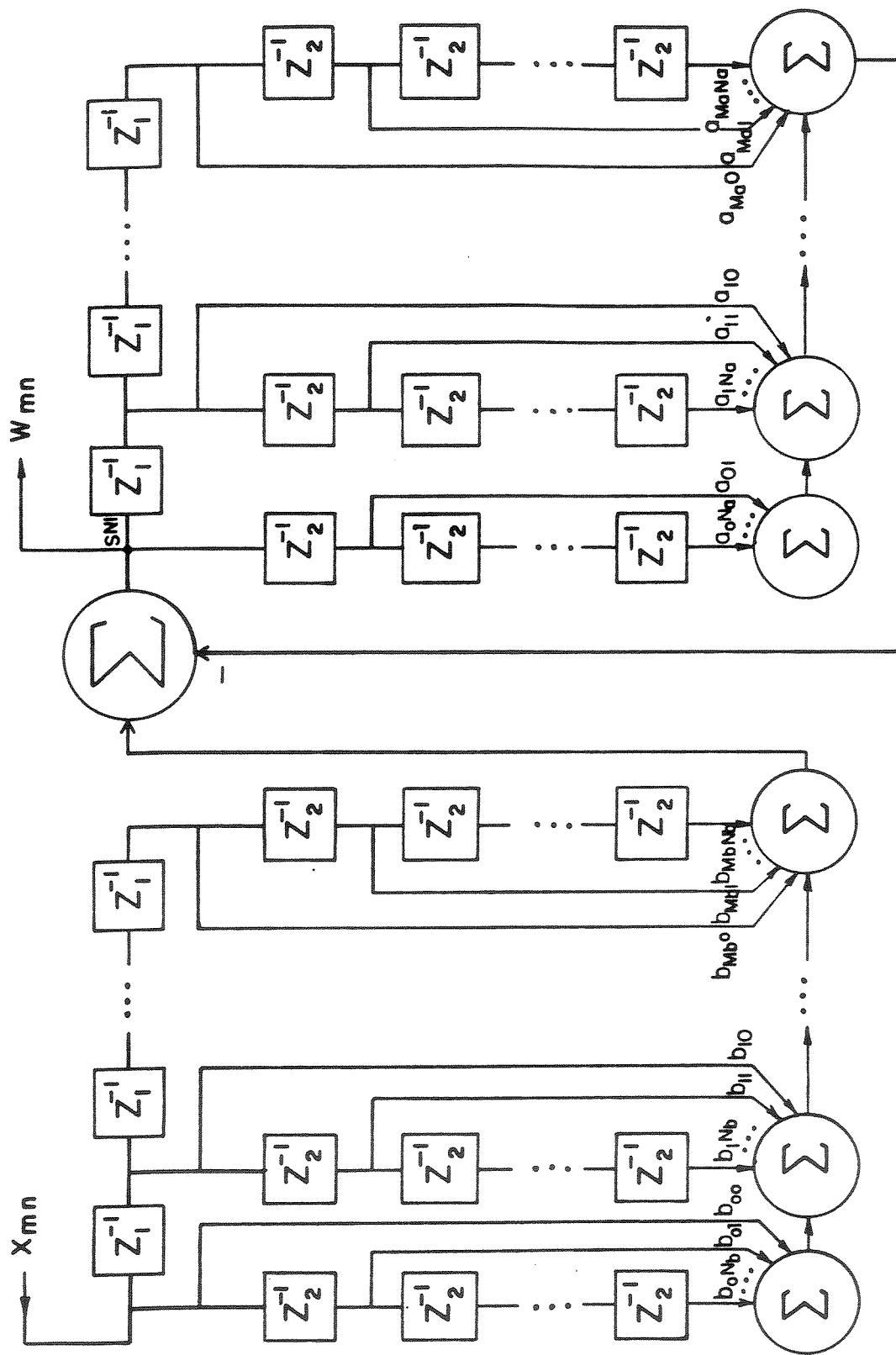


Fig. 1 Block Diagram Representation for Direct Filtering Process

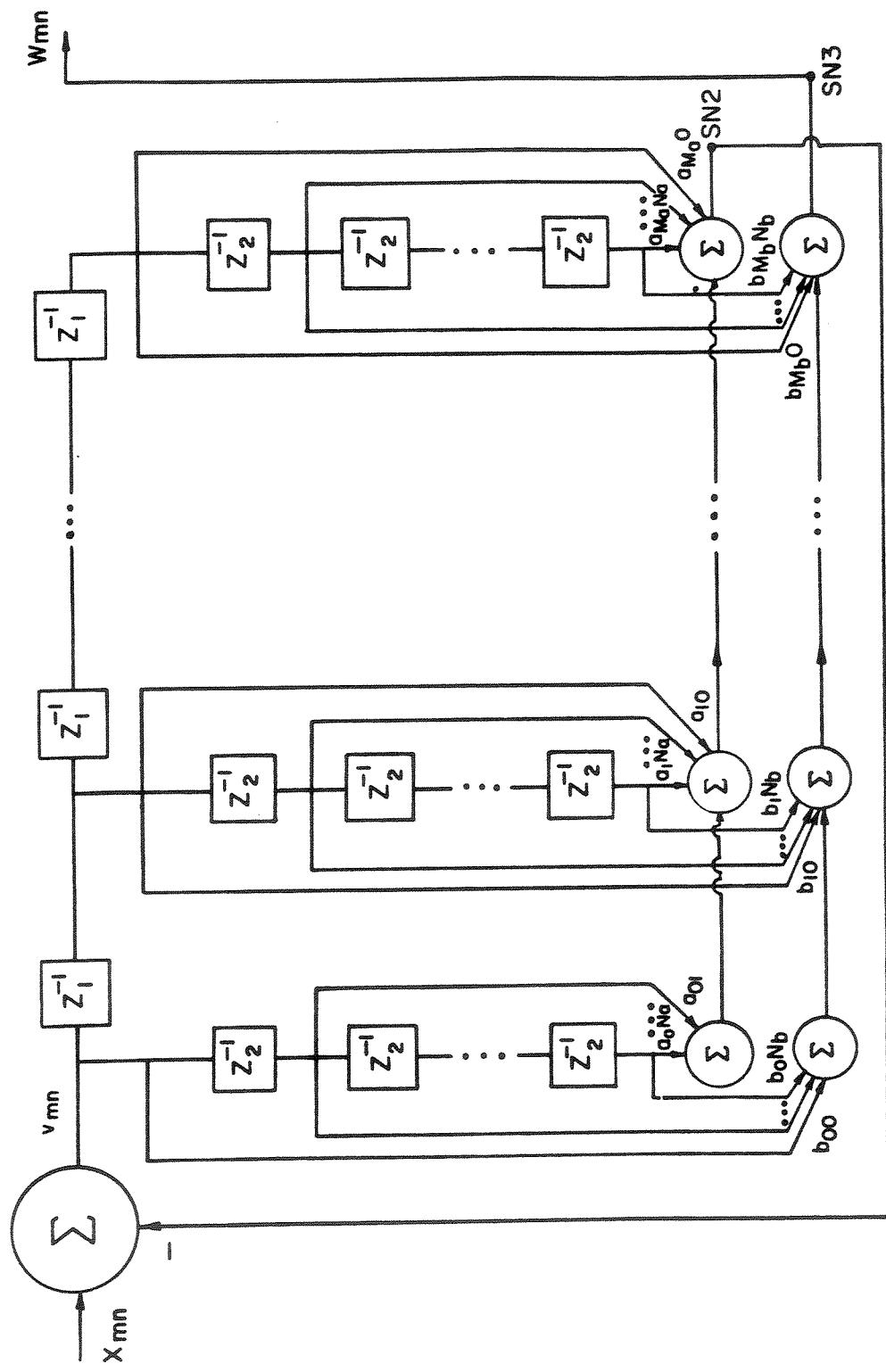


Fig. 2 Block Diagram Representation for Canonic Filtering Process

$$v_{mn} = - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} v_{m-j, n-k} + x_{mn}, \quad (9)$$

$$w_{mn} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} v_{m-j, n-k} \quad (10)$$

where (i)  $m \geq 0$  and  $n \geq 0$ ,

(ii)  $M_b \cdot N_b \leq M_a \cdot N_a$ ,

(iii)  $\{x_{mn}\}$  is the input sequence,

$$x_{jk} = 0, \text{ for } j < 0 \text{ or } k < 0,$$

(iv)  $\{w_{mn}\}$  is the output sequence,

$$w_{jk} = 0, \text{ for } j < 0 \text{ or } k < 0,$$

(v)  $\{v_{mn}\}$  is the state sequence,

$$v_{jk} = v(j, k), \quad j = 0, -1, \dots, -M_a, \quad k = 0, -1, \dots, -N_a, \\ j + k \neq 0,$$

$$v_{jk} = 0, \quad \text{for } j < -M_a \text{ or } k < -N_a.$$

In the following sections, Eq. (2) will be called the "direct filtering process", and Eqs. (9) and (10) the "canonic filtering process".

### Definition:

The "2D sequence mean square average" norm is defined as

$$\langle x \rangle_{p, q}^{K_2, K_1} \triangleq \left( \frac{1}{(K_2-p+1)(K_1-q+1)} \sum_{m=p}^{K_2} \sum_{n=q}^{K_1} |x_{mn}|^2 \right)^{1/2}$$

for every real-valued sequence  $\{x_{mn}\}$ , and every  $K_2, K_1 \in I^+$  and every  $p, q \in I$ , where  $I^+$  is the set of positive integers, and  $I$  is the set of integers.

$[\langle x \rangle_{p,q}^{K_2, K_1}]^2$  is denoted by  $\langle x \rangle_{p,q}^{K_2, K_1}$ .

When both  $p$  and  $q$  are equal to zero,  $p$  and  $q$  are omitted, e.g.,

$\langle x \rangle_{p,q}^{K_2, K_1}$  is denoted by  $\langle x \rangle^{K_2, K_1}$ .

The following lemma is used in the derivation of error bounds.

The proof is given in Appendix I.

### Lemma 1

$$\text{If } f_{mn} = \sum_{k=0}^m \sum_{l=0}^n C_{m-k, n-l} g_{kl}, \text{ for } m \geq 0 \text{ and } n \geq 0$$

$$\text{with } \sum_{k=0}^{\infty} \sum_{l=0}^{\infty} |C_{kl}| < \infty,$$

$$\text{then } \langle f \rangle^{K_2, K_1} \leq \max_{\begin{array}{c} 0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi \end{array}} \left| \sum_{k=0}^{\infty} \sum_{l=0}^{\infty} C_{kl} e^{-ik\omega_1} e^{-il\omega_2} \right| \langle g \rangle^{K_2, K_1}$$

for  $K_1 \geq 0$  and  $K_2 \geq 0$ , where  $i = \sqrt{-1}$ .

We also need the following representations:

$$\sum_{m=0}^{\infty} \sum_{n=0}^{\infty} h_{mn} z_1^{-m} z_2^{-n} = \frac{1}{D(z_1, z_2)}, \quad (11)$$

$$\sum_{m=0}^{\infty} \sum_{n=0}^{\infty} h_{mn}^{(jk)} z_1^{-m} z_2^{-n} = \frac{\sum_{p=j}^{M_a} \sum_{q=k}^{N_a} a_p q z_1^{-(p-j)} z_2^{-(q-k)}}{D(z_1, z_2)}, \quad (12)$$

$j=0, \dots, M_a,$   
 $k=0, \dots, N_a,$   
 $j+k \neq 0.$

### III. ERROR ANALYSIS FOR TWO-DIMENSIONAL DIGITAL FILTERS EMPLOYING FIXED-POINT ARITHMETIC

In this chapter, we analyze the effects of finite word length on two-dimensional digital filters employing fixed-point arithmetic. We first find out the actual system equations with finite word length, and then derive formulas for estimating (1) the output mean squared errors and (2) the output norm error bounds. We only consider the case of roundoff errors. By following a similar approach we can obtain similar results for other sources of error. We study both the direct filtering process and the canonic filtering process.

#### III.1 Actual System Equations with Roundoff Errors

In the implementation of digital filter Eqs. (2), (9), and (10), the finite word length of registers in a general purpose digital computer or special purpose digital hardware produces modification of these difference equations. The actual difference equations corresponding to Eqs. (2), (9), and (10), while taking into account the multiplication roundoff errors, are given here. We assume that:

- (i) each machine number  $q$  is normalized, so that  $|q| < 1$  and is represented by

$$-q_0 + \sum_{k=1}^{t-1} q_k 2^{-k},$$

where  $t$  is the number of bits. The  $q_k$ 's take on values "0" or "1". The following error properties are assumed:

$$f_i[\bar{x}] = \bar{x} + \epsilon = x, \quad |\epsilon| < 2^{-t}, \quad (13)$$

$$f_i[x+y] = x + y, \quad (14)$$

$$f_i[xy] = xy + \delta, \quad |\delta| < 2^{-t}, \quad (15)$$

where  $\bar{x}$  is a real number, and  $x$  and  $y$  are machine numbers. It may be observed that the error  $\delta$  is zero if  $x$  or  $y$  is zero.

(ii) there is no overflow unless otherwise mentioned.

(iii) the numbers  $a_{jk}$ 's,  $b_{jk}$ 's,  $\{x_{mn}\}$ ,  $\{W(-j, -k)\}_{\substack{j=0, k=0 \\ j+k \neq 0}}^{M_a, N_a}$

and  $\{V(-j, -k)\}_{\substack{j=0, k=0 \\ j+k \neq 0}}^{M_a, N_a}$  are machine numbers.

(iv) the digital filter of Eq. (2) or (9) and (10) is stable ([1], [2]), and we let

$$fi[b_{jk} x_{m-j, n-k}] = b_{jk} x_{m-j, n-k} + \delta_{mn, jk}$$

$$fi[a_{jk} y_{m-j, n-k}] = a_{jk} y_{m-j, n-k} + \eta_{mn, jk}$$

$$fi[b_{jk} u_{m-j, n-k}] = b_{jk} u_{m-j, n-k} + \gamma_{mn, jk}$$

$$fi[a_{jk} u_{m-j, n-k}] = a_{jk} u_{m-j, n-k} + \epsilon_{mn, jk}$$

where the symbols  $\delta_{mn, jk}$ ,  $\eta_{mn, jk}$ ,  $\gamma_{mn, jk}$  and  $\epsilon_{mn, jk}$  play the same role as  $\delta$  in Eq. (15) above, and take on values in the interval  $(-2^{-t}, 2^{-t})$ . The ordering of the arithmetic operations of Eqs. (2), (9) and (10) are according to the flow graphs shown in Figures 3 and 4.

The above assumptions lead to the following actual system of equations:

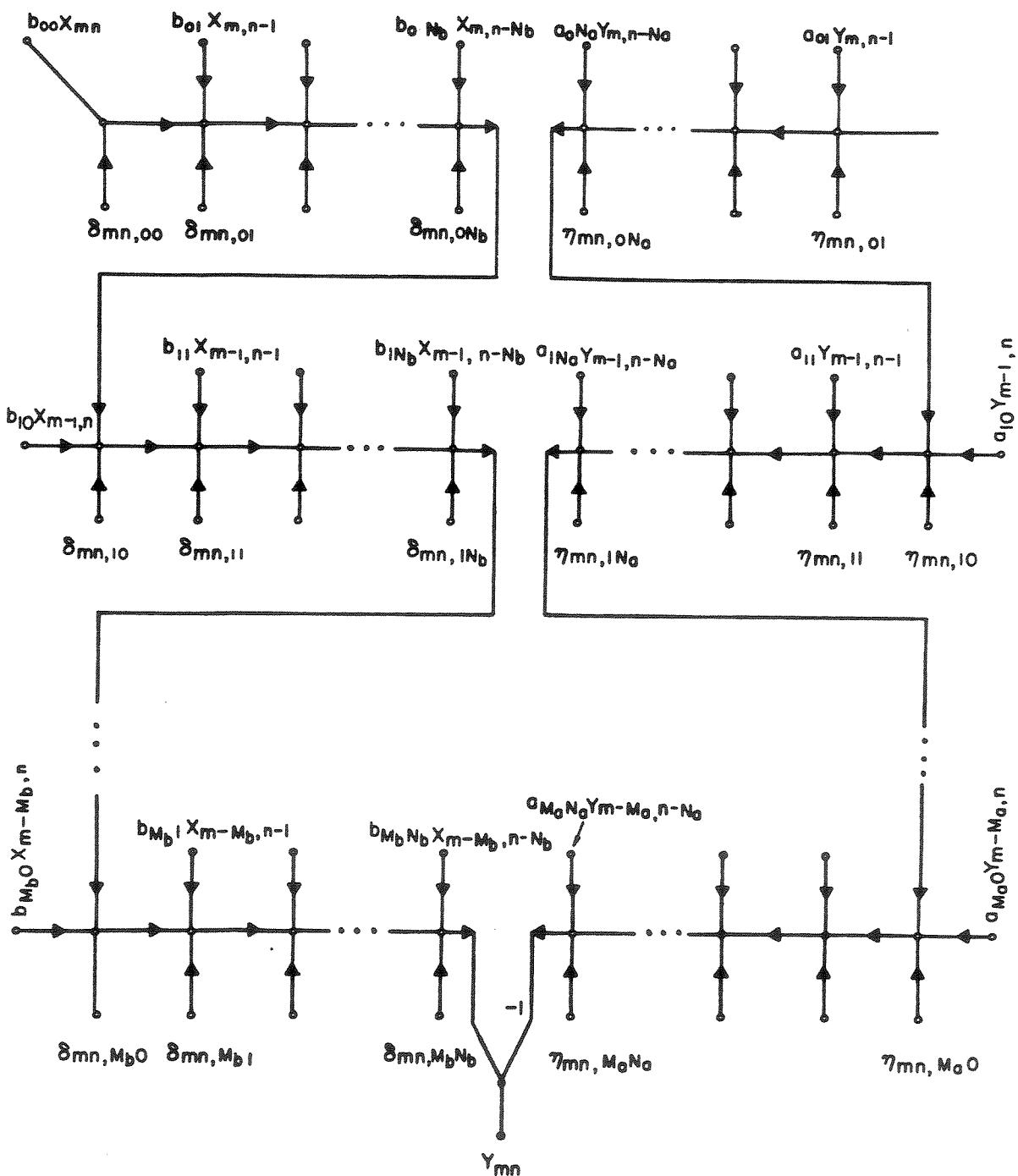


Fig. 3 Flow Graph for Fixed-Point Direct Filtering Process

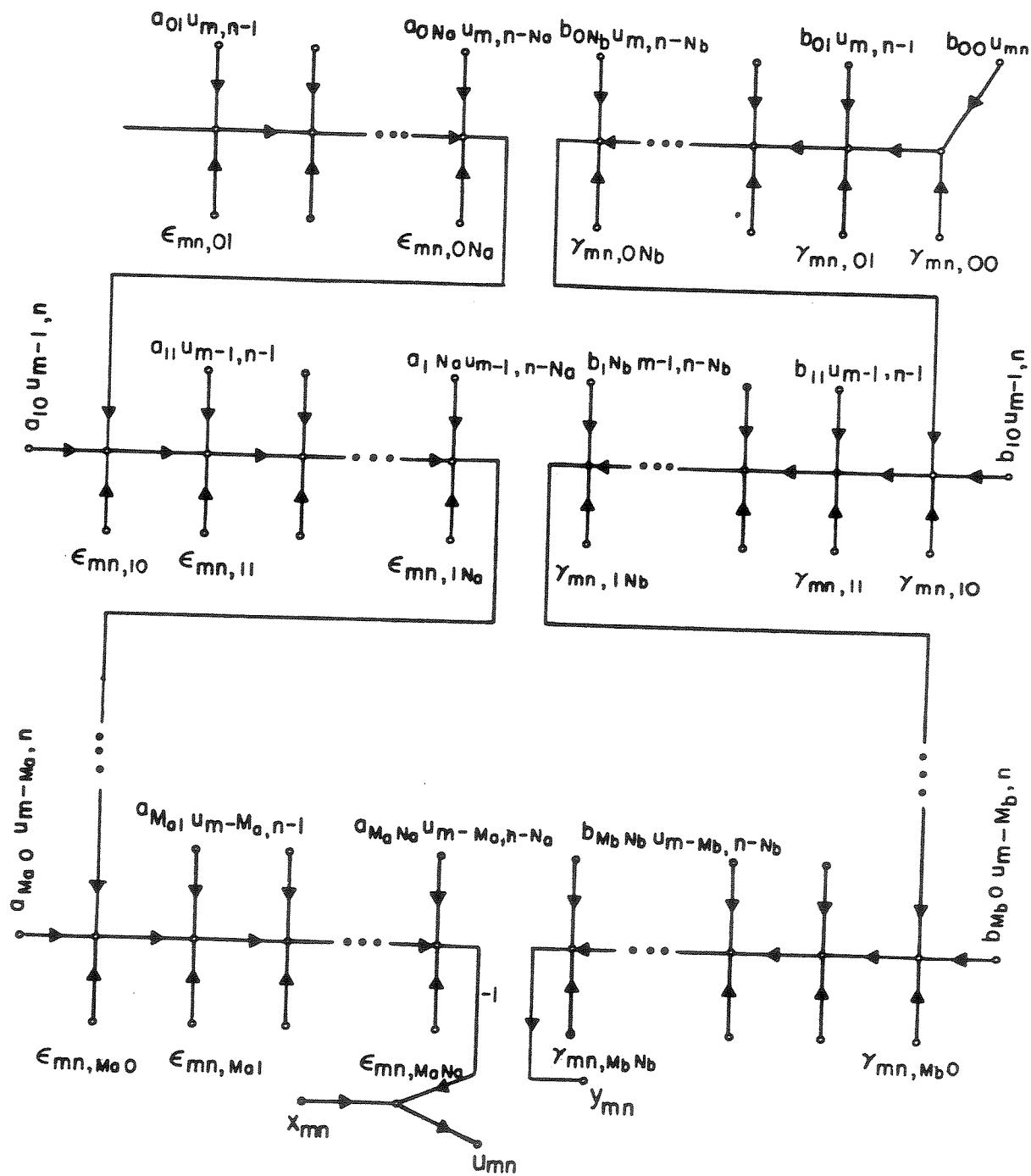


Fig. 4 Flow Graph for Fixed-Point Canonic Filtering Process

## (1) Direct Filtering Process

$$\begin{aligned}
 y_{mn} &= f_1 \left[ \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} x_{m-j, n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} y_{m-j, n-k} \right] \\
 &= \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} x_{m-j, n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} y_{m-j, n-k} \\
 &\quad + e_{mn}^{(d)}, \quad m \geq 0 \text{ and } n \geq 0,
 \end{aligned} \tag{16}$$

where

$$e_{mn}^{(d)} = \begin{cases} \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} \delta_{mn, jk} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} \eta_{mn, jk}, & \text{for } m \geq 0 \text{ and } n \geq 0, \\ 0, & \text{otherwise,} \end{cases} \tag{17}$$

## (2) Canonic Filtering Process

$$\begin{aligned}
 u_{mn} &= f_1 \left[ - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} u_{m-j, n-k} + x_{mn} \right] \\
 &= - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} u_{m-j, n-k} + e_{mn}^{(1)} + x_{mn}, \quad \text{for } m \geq 0 \text{ and } n \geq 0,
 \end{aligned} \tag{18}$$

$$\begin{aligned}
 y_{mn} &= f_i \left[ \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} u_{m-j, n-k} \right] \\
 &= \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} u_{m-j, n-k} + e_{mn}^{(2)}, \text{ for } m \geq 0 \text{ and } n \geq 0, \quad (19)
 \end{aligned}$$

where

$$e_{mn}^{(1)} = \begin{cases} - \sum_{j=0}^{M_a} \sum_{k=0}^{N_a} e_{mn, jk}, & m \geq 0 \text{ and } n \geq 0, \\ 0, & j + k \neq 0 \\ 0, & \text{otherwise,} \end{cases} \quad (20)$$

$$e_{mn}^{(2)} = \begin{cases} \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} y_{mn, jk}, & m \geq 0 \text{ and } n \geq 0, \\ 0, & \text{otherwise.} \end{cases} \quad (21)$$

### III.2 Error Analysis

#### III.2.1 Behavior of the Sources of Error

##### Roundoff Error Accumulation

Let

$$e_{mn} = y_{mn} - w_{mn}, \quad (22)$$

$$e'_{mn} = u_{mn} - v_{mn}. \quad (23)$$

Then, for the direct filtering process, by Eqs. (2) and (16),

$$e_{mn} = - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} e_{m-j, n-k} + e_{mn}^{(d)}, \quad (24)$$

or

$$\sum_{j=0}^{M_a} \sum_{k=0}^{N_a} a_{jk} e_{m-j, n-k} = e_{mn}^{(d)}, \text{ with } a_{00} = 1, \quad (25)$$

and for the canonic filtering process, by Eqs. (9), (10), (18) and (19),

$$e_{mn} = - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} e_{m-j, n-k} + e_{mn}^{(1)} \quad (26)$$

or

$$\sum_{j=0}^{M_a} \sum_{k=0}^{N_a} a_{jk} e_{m-j, n-k} = e_{mn}^{(1)}, \text{ with } a_{00} = 1, \quad (27)$$

$$e_{mn} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} e_{m-j, n-k} + e_{mn}^{(2)}. \quad (28)$$

Equations (24), (25), (26), (27) and (28) can be best illustrated by Figures 5(a) and 6(a), where the roundoff errors  $\{e_{mn}^{(d)}\}$ ,  $\{e_{mn}^{(1)}\}$ , and  $\{e_{mn}^{(2)}\}$  act as noise sources injected at the indicated junctions.

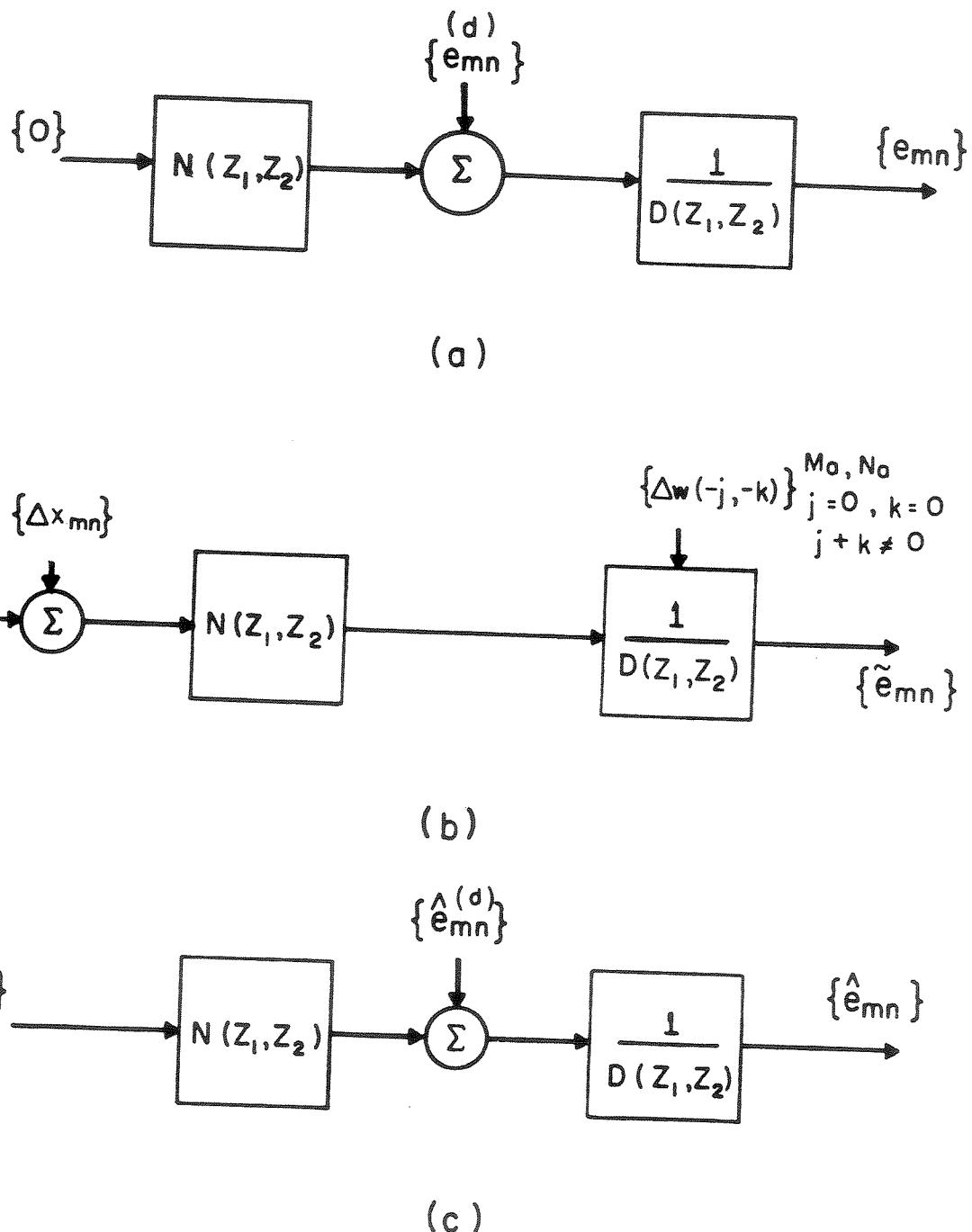
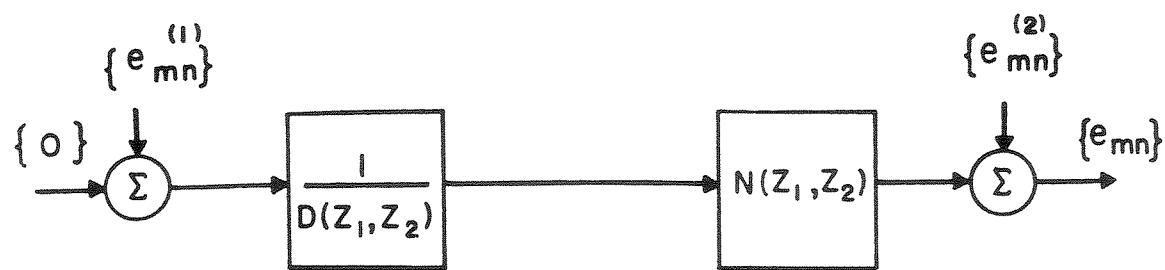
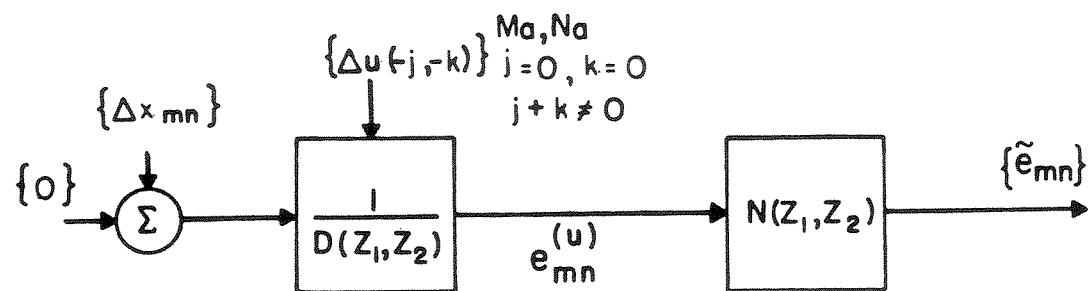


Fig. 5 Block Diagram Interpretations for Direct Filtering Process

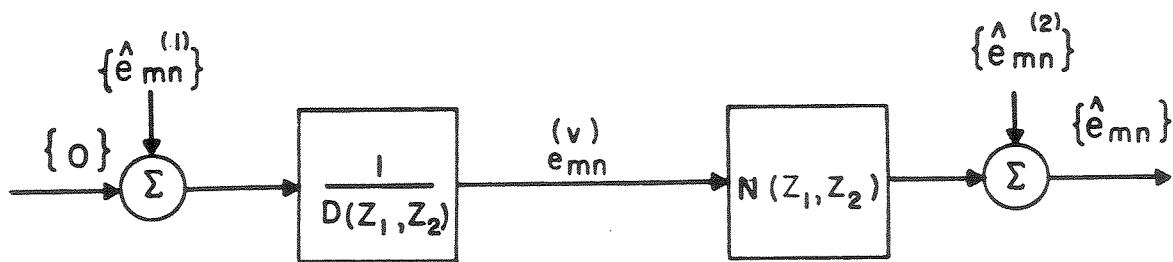
- (a) Error  $\{e_{mn}\}$  due to roundoff
- (b) Error  $\{\tilde{e}_{mn}\}$  due to quantization of inputs and initial values
- (c) Error  $\{\hat{e}_{mn}\}$  due to coefficient quantization



(a)



(b)



(c)

Fig. 6 Block Diagram Interpretations for Canonic Filtering Process

- (a) Error  $\{e_{mn}\}$  due to roundoff
- (b) Error  $\tilde{e}_{mn}$  due to quantization of inputs and initial values
- (c) Error  $\hat{e}_{mn}$  due to coefficient quantization

### Input and Initial Value Quantization

An interpretation similar to the above is possible for input quantization and initial state quantization. Let the symbols with bars denote infinite precision quantities. For the direct filtering process, the use of the following notation makes the interpretation of noise sources in Figure 5(b) obvious.

$$(i) \Delta x_{mn} \triangleq \begin{cases} x_{mn} - \bar{x}_{mn}, & m \geq 0 \text{ and } n \geq 0, \\ 0, & \text{otherwise,} \end{cases}$$

$$(ii) \Delta w(j,k) \triangleq W(j,k) - \bar{W}(j,k), \quad |\Delta w(j,k)| \leq 2^{-t},$$

$$(iii) \tilde{e}_{mn} \triangleq \begin{cases} w_{mn} - \bar{w}_{mn}, & m \geq 0 \text{ and } n \geq 0, \\ \Delta w(m,n), & m = 0, -1, \dots, -M_a, \\ & n = 0, -1, \dots, -N_a, \quad m + n \neq 0, \\ 0, & \text{for } m < -M_a \text{ or } n < -N_a. \end{cases}$$

For the canonic filtering process, the use of the following additional notation is needed for suitable interpretation of Figure 6(b).

$$(iv) \Delta u(j,k) \triangleq u(j,k) - \bar{V}(j,k), \quad |\Delta V(j,k)| \leq 2^{-t},$$

$$(v) e_{mn}^{(u)} \triangleq \begin{cases} u_{mn} - \bar{u}_{mn}, & m \geq 0, \quad n \geq 0, \\ \Delta u(m,n), & \text{for } m = 0, -1, \dots, -M_a, \\ & n = 0, -1, \dots, -N_a, \quad m + n \neq 0, \\ 0 & \text{for } m < -M_a \text{ or } n < -N_a, \end{cases}$$

$$(vi) \tilde{e}_{mn} = w_{mn} - \bar{w}_{mn}, \quad m \geq 0, \quad n \geq 0.$$

### Coefficient Quantization

Finally, the coefficient quantization introduces output errors as shown in Figures 5(c) and 6(c) for direct and canonic filtering processes, respectively, with the following notation.

$$(vii) \Delta b_{jk} \triangleq b_{jk} - \bar{b}_{jk},$$

$$\Delta a_{jk} \triangleq a_{jk} - \bar{a}_{jk},$$

$$|\Delta b_{jk}| \leq 2^{-t}, \quad |\Delta a_{jk}| \leq 2^{-t},$$

$$(viii) \hat{e}_{mn}^{(d)} \triangleq \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} \Delta b_{jk} x_{m-j, n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} \Delta a_{jk} w_{m-j, n-k},$$

$$(ix) \hat{e}_{mn}^{(1)} \triangleq - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} \Delta a_{jk} v_{m-j, n-k},$$

$$\hat{e}_{mn}^{(2)} \triangleq \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} \Delta b_{jk} v_{m-j, n-k},$$

$$(x) e_{mn}^{(v)} = v_{mn} - \bar{v}_{mn}, \quad m \geq 0, \quad n \geq 0,$$

$$\hat{e}_{mn} = w_{mn} - \bar{w}_{mn}, \quad m \geq 0, \quad n \geq 0.$$

In the later developments, output error bounds due to roundoff error accumulation are derived, mean-square-error analysis is presented, and dynamic range is also discussed. By following the same line of development, similar results for the effects of quantization errors for input and initial conditions, coefficients, and of the combinations of more than two sources of these errors (including roundoff errors) can be obtained without serious difficulty.

### III.2.2 Mean Squared Error Analysis

Under certain circumstances, it is reasonable to model the effect of the rounding at each multiplication by the introduction of a white-noise source uniformly distributed with amplitude in the interval  $(-E_o/2, E_o/2)$  (i.e. the mean is zero, and the variance is  $E_o^2/12$ ) where  $E_o$  is the quantization level. Each of the noise sources is assumed to be independent of each other and of the input. Figure 7 shows how the quantization noise is introduced into the block diagram representation of a second order filter. The noise sources can be replaced by a single noise source as

$$e_{mn} = e_{mn,1} + e_{mn,2} + e_{mn,3}.$$

In general, from Eqs. (17), (20) and (21) the sources of roundoff errors can be represented by single sources  $e_{mn}^{(d)}$ ,  $e_{mn}^{(1)}$ , and  $e_{mn}^{(2)}$  with zero means and with variances as follows:

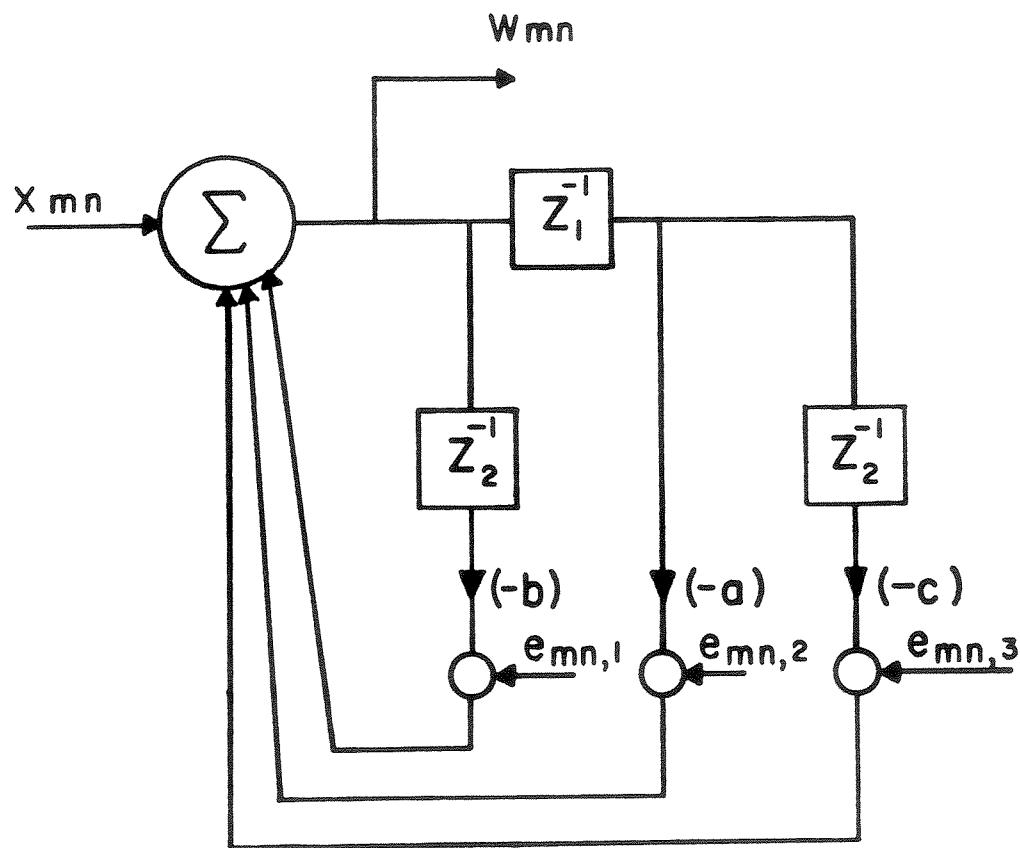
$$\sigma_{e^{(d)}}^2 = \frac{E_o^2}{12} (\hat{M}_a \cdot \hat{N}_a - 1 + \hat{M}_b \cdot \hat{N}_b) , \quad (29)$$

$$\sigma_{e^{(1)}}^2 = \frac{E_o^2}{12} (\hat{M}_a \cdot \hat{N}_a - 1) , \quad (30)$$

$$\sigma_{e^{(2)}}^2 = \frac{E_o^2}{12} (\hat{M}_b \cdot \hat{N}_b) , \quad (31)$$

where  $\hat{M}_b = M_b + 1$ ,  $\hat{N}_b = N_b + 1$ ,  $\hat{M}_a = M_a + 1$ ,  $\hat{N}_a = N_a + 1$ , and we have assumed that none of the coefficients, a's and b's, are zero or 1. If any of the coefficients are zero, the error is suitably reduced. We hold this assumption throughout the rest of this chapter.

The output  $f_{mn}$ , when the input consists of the noise samples  $r_{mn}$ , is



$$\text{Fig. 7 } G(z_1, z_2) = \frac{1}{1 + az_1^{-1} + bz_2^{-1} + cz_1^{-1}z_2^{-1}}$$

$$f_{mn} = \sum_{j=0}^m \sum_{k=0}^n h_{jk} r_{m-j, n-k} = \sum_{j=0}^m \sum_{k=0}^n h_{m-j, n-k} r_{jk} \quad (32)$$

where  $\{h_{mn}\}$  is the point spread response. Thus, for the direct filtering process,

$$E\{f_{mn}^2\} = \frac{E_o^2}{12} (\hat{M}_a \cdot \hat{N}_a^{-1} + \hat{M}_b \cdot \hat{N}_b) \sum_{j=0}^m \sum_{k=0}^n h_{jk}^2 . \quad (33)$$

For the steady state condition,

$$\sigma_t^2 = \frac{E_o^2}{12} (\hat{M}_a \cdot \hat{N}_a^{-1} + \hat{M}_b \cdot \hat{N}_b) \sum_{j=0}^{\infty} \sum_{k=0}^{\infty} h_{jk}^2 . \quad (34)$$

Generally, regardless of the configuration of the filters, if the impulse response from the  $(jk)$ th noise source to the output is  $\{h_{mn, jk}\}_{m=0}^{\infty},_{n=0}^{\infty}$ , then the steady state output-noise variance due to the  $(jk)$ th noise source is

$$\sigma_{jk}^2 = \frac{E_o^2}{12} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} h_{mn, jk}^2 \quad (35)$$

and the total output noise is

$$\sigma_t^2 = \sum_j \sum_k \sigma_{jk}^2 . \quad (36)$$

### III.2.3 Norm Error Bounds

In this section we first derive the absolute upper bounds for output errors. We also obtain the corresponding expectation bounds. From Eq. (17), it follows that

$$|e_{mn}^{(d)}| \leq 2^{-t} (\hat{M}_b \cdot \hat{N}_b + \hat{M}_a \cdot \hat{N}_a - 1) \quad (37)$$

or

$$\langle e^{(d)} \rangle^{K_2, K_1} \leq 2^{-t} (\hat{M}_b \cdot \hat{N}_b + \hat{M}_a \cdot \hat{N}_a - 1). \quad (38)$$

Further, from Eq. (24) it follows that

$$e_{mn} = \sum_{j=0}^m \sum_{k=0}^n h_{m-j, n-k} e_{mn}^{(d)}. \quad (39)$$

Thus the bound for the total roundoff error at the output for the direct filtering process is

$$\begin{aligned} \langle e \rangle^{K_2, K_1} &\leq \max_{\substack{0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi}} |D^{-1}(e^{i\omega_1}, e^{i\omega_2})| \langle e^{(d)} \rangle^{K_2, K_1} \\ &\leq 2^{-t} (\hat{M}_b \cdot \hat{N}_b + \hat{M}_a \cdot \hat{N}_a - 1) \cdot \max_{\substack{0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi}} |D^{-1}(e^{i\omega_1}, e^{i\omega_2})| \end{aligned} \quad (40)$$

by lemma 1 where  $K_1, K_2 \geq 0$ . For the canonic filtering process

$$|e_{mn}^{(1)}| \leq 2^{-t} (\hat{M}_a \cdot \hat{N}_a - 1), \quad (41)$$

$$|e_{mn}^{(2)}| \leq 2^{-t} (\hat{M}_b \cdot \hat{N}_b), \quad (42)$$

or

$$\langle e^{(1)} \rangle^{K_2, K_1} \leq 2^{-t} (\hat{M}_a \cdot \hat{N}_a - 1), \quad (43)$$

$$\langle e^{(2)} \rangle^{K_2, K_1} \leq 2^{-t} (\hat{M}_b \cdot \hat{N}_b). \quad (44)$$

The total roundoff error  $\{e_{mn}\}$  accumulated at the output is given by

$$e_{mn} = \sum_{j=0}^m \sum_{k=0}^n g_{m-j, n-k} e_{mn}^{(1)} + e_{mn}^{(2)}, \quad (45)$$

and by lemma 1

$$\langle e - e^{(2)} \rangle^{K_2, K_1} \leq \max_{\begin{array}{l} 0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi \end{array}} |G(e^{i\omega_1}, e^{i\omega_2})| \langle e^{(1)} \rangle^{K_2, K_1}. \quad (46)$$

Inserting (43) and (44) into (46), one obtains

$$\langle e \rangle^{K_2, K_1} \leq \max_{\begin{array}{l} 0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi \end{array}} |G(e^{i\omega_1}, e^{i\omega_2})| \cdot 2^{-t}(\hat{M}_a \cdot \hat{N}_a - 1) + 2^{-t}(\hat{M}_b \cdot \hat{N}_b). \quad (47)$$

Eqs. (40) and (47) are absolute upper bounds. If we keep the assumptions for the absolute errors  $\delta_{mn, jk}, \eta_{mn, jk}, \dots$ , etc. in the beginning of Section III.2.2, we can easily obtain the following expectation bounds by the application of lemma 1 to Eqs. (39) and (45);

$$\begin{aligned} E\{^2 \langle e \rangle^{K_2, K_1}\} &\leq \frac{E_0^2}{12} (\hat{M}_b \cdot \hat{N}_b + \hat{M}_a \cdot \hat{N}_a - 1) \\ &\cdot \max_{\begin{array}{l} 0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi \end{array}} |D^{-1}(e^{i\omega_1}, e^{i\omega_2})|^2 \end{aligned} \quad (48)$$

for the direct filtering process, and

$$\begin{aligned} E\{^2 \langle e \rangle^{K_2, K_1}\} &\leq \frac{E_0^2}{12} [(\hat{M}_a \cdot \hat{N}_a - 1) \max_{\begin{array}{l} 0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi \end{array}} |G(e^{i\omega_1}, e^{i\omega_2})|^2 \\ &+ \hat{M}_b \cdot \hat{N}_b] \end{aligned} \quad (49)$$

for the canonic filtering process.

### III.3 Dynamic Range Considerations

Overflow occurs when the absolute value of the sum of more than one signal is greater than 1. For the two 2D fixed-point digital filtering processes discussed above inputs must be properly scaled so that overflow will not occur at node SN1 for the direct process shown in Figure 1, and at nodes SN2 and SN3 for the canonic process shown in Figure 2. The maximum value of input signal that will not cause overflow is found for each case as follows.

#### III.3.1 Direct Filtering Process

At SN1 in Figure 1,

$$w_{mn} = \sum_{j=0}^m \sum_{k=0}^n x_{m-j, n-k} g_{jk}$$

where

$$\sum_{j=0}^{\infty} \sum_{k=0}^{\infty} g_{jk} z_1^{-j} z_2^{-k} = \frac{N(z_1, z_2)}{D(z_1, z_2)},$$

and

$$\begin{aligned} |w_{mn}| &\leq \sum_{j=0}^m \sum_{k=0}^n |x_{m-j, n-k}| |g_{jk}| \\ &\leq \sum_{j=0}^{\infty} \sum_{k=0}^{\infty} |x_{m-j, n-k}| |g_{jk}| \\ &\leq x_{\max d} \sum_{j=0}^{\infty} \sum_{k=0}^{\infty} |g_{jk}| \end{aligned}$$

where

$$|x_{jk}| \leq x_{\max d}, \text{ for all } j \text{ and } k.$$

In order to guarantee  $|w_{mn}| < 1$  for every  $m \geq 0$  and  $n \geq 0$ , it suffices to have

$$x_{\max d} \leq \frac{1}{\sum_{j=0}^{\infty} \sum_{k=0}^{\infty} |g_{jk}|} . \quad (50)$$

### III.3.2 Canonic Filtering Process

At SN2 in Figure 2,

$$v_{mn} = \sum_{j=0}^m \sum_{k=0}^n x_{m-j, n-k} h_{jk}$$

where

$$\sum_{j=0}^{\infty} \sum_{k=0}^{\infty} h_{jk} z_1^{-j} z_2^{-k} = \frac{1}{D(z_1, z_2)}$$

so,

$$|v_{mn}| \leq x_{\max c} \cdot \sum_{j=0}^{\infty} \sum_{k=0}^{\infty} |h_{jk}| . \quad (51)$$

At SN3,

$$w_{mn} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} v_{m-j, n-k}$$

so,

$$|w_{mn}| \leq v_{\max} \cdot \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} |b_{jk}| .$$

Let

$$v_{\max} \leq \frac{1}{\sum_{j=0}^{M_b} \sum_{k=0}^{N_b} |b_{jk}|} , \quad (52)$$

then  $|w_{mn}| < 1$  for every  $m > 0$  and  $n > 0$

where  $|x_{jk}| < x_{\max c}$  and  $|v_{jk}| < v_{\max}$ , for every  $j \geq 0$  and  $k \geq 0$ .

From Eqs. (51) and (52), we have

$$|x_{mn}| < x_{\max} \leq \frac{1}{\sum_{j=0}^{\infty} \sum_{k=0}^{\infty} |h_{jk}|} \times \frac{1}{\sum_{j=0}^{M_b} \sum_{k=0}^{N_b} |b_{jk}|}, \quad (53)$$

for  $m \geq 0$  and  $n \geq 0$ , and for no overflows at SN2 and SN3. It may be observed and emphasized that these are worst case bounds.

### III.4 Numerical Results

We have a decimal simulation scheme to simulate the filtering operations. All the quantities involved are in double precision. The finite bit operations are simulated by having a decimal quantizer with quantization level  $E_0 = 2^{-(t-1)}$  follow each multiplication (or each input signal).

When there is no quantizer, the results are taken as infinite precision ones. For the CDC 6600 computer, the mantissa of a number is represented by 48 bits. When double precision is used, the maximum possible error for the mantissa is  $2^{-97} \approx 10^{-30}$ . The following two examples are given to demonstrate the usefulness of the analytic results stated in Eqs. (35), (36), and (40) and (47). Table 1 and Table 2 show the computer results for the operations from  $m = 1$  and  $n = 1$  to  $m = 100$  and  $n = 100$ . The impulse response in each example is reasonably small beyond  $m = 100$  and  $n = 100$ .

Columns (I) and (III) list the "actual maximum errors" and "actual mean-square errors" calculated by the decimal simulation scheme on executing Eqs. (2), (9), and (10) respectively. Column (II) gives "theoretical

upper bound of errors" by Eqs. (40) and (47). The actual error sequence mean square average norms are obtained by taking the square roots of corresponding values in Column (III). Column (IV) gives "theoretical mean-square errors" by Eqs. (35) and (36), respectively. Inputs in both cases are arbitrarily selected.

Example 1.

$$G(z_1, z_2) = \frac{1}{1 - 0.7z_1^{-1} - 0.5z_2^{-1} + 0.3z_1^{-1}z_2^{-1}},$$

(This filter is given in [2]),

input:  $x_{mn} = 0.1 \cos(\omega t)$  where  $\omega t = 0.01 m(n-1)\pi$ .

The point spread response dies out slowly. The real theoretical values should be greater than the ones listed in Column (IV).

Table 1

items bits	(I)	(II)	(III)	(IV)
t = 8	$3.38867 \times 10^{-2}$	$1.17188 \times 10^{-1}$	$8.73152 \times 10^{-5}$	$4.54929 \times 10^{-5}$
t = 12	$1.91280 \times 10^{-3}$	$7.32422 \times 10^{-3}$	$3.04815 \times 10^{-7}$	$1.77707 \times 10^{-7}$
t = 16	$1.24287 \times 10^{-4}$	$4.57764 \times 10^{-4}$	$1.08707 \times 10^{-9}$	$6.94167 \times 10^{-10}$
t = 20	$8.71887 \times 10^{-6}$	$2.86102 \times 10^{-5}$	$4.59030 \times 10^{-12}$	$2.71159 \times 10^{-12}$
t = 24	$4.94035 \times 10^{-7}$	$1.78814 \times 10^{-6}$	$1.82150 \times 10^{-14}$	$1.05921 \times 10^{-14}$
t = 28	$3.09238 \times 10^{-8}$	$1.11759 \times 10^{-6}$	$6.54997 \times 10^{-17}$	$4.13756 \times 10^{-17}$
t = 32	$2.05030 \times 10^{-9}$	$6.98492 \times 10^{-9}$	$2.75747 \times 10^{-19}$	$1.61623 \times 10^{-19}$

Example 2.

$$G(z_1, z_2) = \frac{N(z_1, z_2)}{D(z_1, z_2)}$$

where

$$N(z_1, z_2) = 1 - 0.474999z_2^{-1} - 0.636396z_1^{-1} + 0.302287z_1^{-1}z_2^{-1},$$

$$D(z_1, z_2) = 1 - 0.949998z_2^{-1} + 0.9025z_2^{-2} + 1.27279z_1^{-1}$$

$$- 1.20915z_1^{-1}z_2^{-1} + 1.14869z_1^{-1}z_2^{-2} + 0.81z_1^{-2}$$

$$- 0.769498z_1^{-2}z_2^{-1} + 0.731025z_1^{-2}z_2^{-2},$$

input:  $x_{mn} = 0.025 \cos \omega t$  and

$$\omega t = 0.1\pi \times [(m-1) \times 100 + n] + 0.01n.$$

The value of maximum gain of this filter is approximately 60.

Table 2

Items bits	(I)		(II)		(III)		(IV)	
	Direct Process	Canonic Process	Direct Process	Canonic Process	Direct Process	Canonic Process	Direct Process	Canonic Process
t = 8	2.19017 $\times 10^{-1}$	2.05563 $\times 10^{-1}$	3.78207	1.70522	3.02690 $\times 10^{-3}$	2.70298 $\times 10^{-3}$	2.31123 $\times 10^{-3}$	2.91967 $\times 10^{-3}$
t = 12	1.04947 $\times 10^{-2}$	1.34391 $\times 10^{-2}$	2.36280 $\times 10^{-1}$	1.06576 $\times 10^{-1}$	6.14841 $\times 10^{-6}$	1.06663 $\times 10^{-5}$	9.02825 $\times 10^{-6}$	1.14050 $\times 10^{-5}$
t = 16	6.96397 $\times 10^{-4}$	7.42209 $\times 10^{-4}$	1.47737 $\times 10^{-2}$	6.66101 $\times 10^{-3}$	2.86827 $\times 10^{-8}$	4.37726 $\times 10^{-8}$	3.52666 $\times 10^{-8}$	4.45507 $\times 10^{-8}$
t = 20	4.64883 $\times 10^{-5}$	4.49094 $\times 10^{-5}$	9.23358 $\times 10^{-4}$	4.16312 $\times 10^{-4}$	1.09832 $\times 10^{-10}$	1.42745 $\times 10^{-10}$	1.37760 $\times 10^{-10}$	1.74026 $\times 10^{-10}$
t = 24	2.64667 $\times 10^{-6}$	3.04092 $\times 10^{-6}$	5.77099 $\times 10^{-5}$	2.60196 $\times 10^{-5}$	4.47297 $\times 10^{-13}$	5.33565 $\times 10^{-13}$	5.38126 $\times 10^{-13}$	6.79790 $\times 10^{-13}$
t = 28	1.93636 $\times 10^{-7}$	2.04656 $\times 10^{-7}$	3.60687 $\times 10^{-6}$	1.62622 $\times 10^{-6}$	2.36728 $\times 10^{-15}$	2.55708 $\times 10^{-15}$	2.10205 $\times 10^{-15}$	2.65543 $\times 10^{-15}$
t = 32	1.04461 $\times 10^{-8}$	1.06558 $\times 10^{-8}$	2.25429 $\times 10^{-7}$	1.01639 $\times 10^{-7}$	6.99403 $\times 10^{-18}$	7.58707 $\times 10^{-18}$	8.21114 $\times 10^{-18}$	1.03728 $\times 10^{-17}$

#### IV. ERROR ANALYSIS FOR TWO-DIMENSIONAL DIGITAL FILTERS EMPLOYING FLOATING-POINT ARITHMETIC

In this chapter, we analyze the effects of finite word length for two-dimensional digital filters employing floating-point arithmetic. Our procedures are basically the same as in Chapter III. We present a systematic way of estimating (1) the output mean squared errors and (2) the output norm error bounds for all three sources of error. Extensive numerical experiments show that the method leads to satisfactory results. We concentrate our efforts on the direct filtering process of Eq. (2). We begin by deriving the actual system equations with finite word length.

##### IV.1 Actual Systems of Equations

###### Basic Assumptions for Digital Filters

(1) each machine number  $q$  is equal to " $\text{sgn}(q) \cdot a \cdot 2^b$ " where the exponent " $b$ " is an integer and " $a$ ", the mantissa, is represented by a  $t$  bit number. " $a$ " takes on values in  $[\frac{1}{2}, 1)$  or  $\{0\}$ . The following error properties are true under this assumption;

$$\text{fl } [x] = x(1 + \epsilon), \quad |\epsilon| < 2^{-t}, \quad (54)$$

$$\text{fl } [x+y] = (x+y)(1 + \rho), \quad |\rho| < 2^{-t}, \quad (55)$$

$$\text{fl } [xy] = xy(1 + \delta), \quad |\delta| < 2^{-t}, \quad (56)$$

where  $x$  and  $y$  are infinite precision numbers,  $\epsilon$ ,  $\rho$ , and  $\delta$  are relative errors, and  $\text{fl} [\cdot]$  denotes the floating-point operation with  $t$ -bit mantissa,

(2) the range of the values of  $b$  is adequate enough to ensure that all the computed numbers lie within the permissible range,

(3) the digital filter of Eq. (2) is stable ([1], [2]).

(4) the ordering of the arithmetic operations is according to the flow diagram shown in Figure 8, where  $\delta_{mn,ij}$ ,  $\epsilon_{mn,ij}$ ,  $r_{mn,ij}$ ,  $\xi_{mn}$

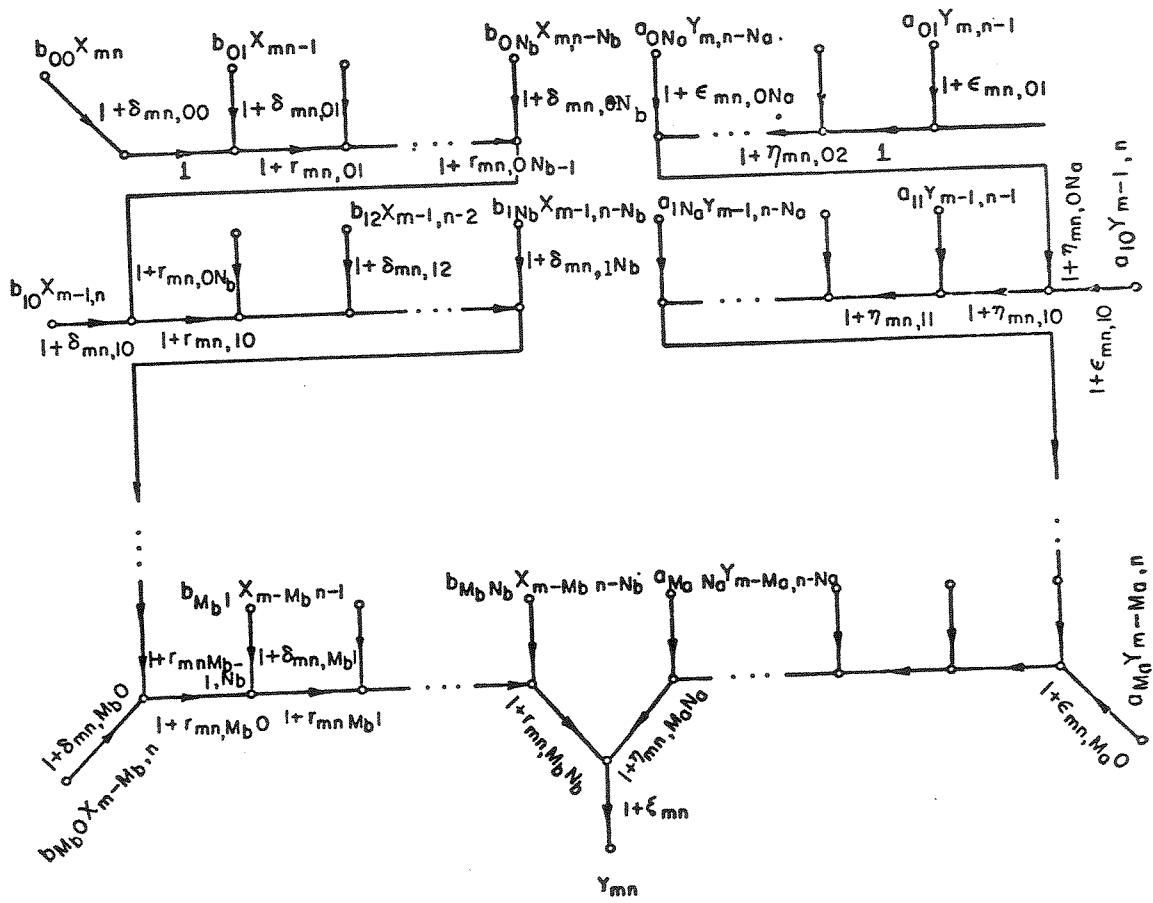


Fig. 8 Flow Graph for Floating-point Direct Filtering Process

$\eta_{mn,ij}$  are relative errors and take on values in  $(-2^{-t}, 2^{-t})$ .

Actual System of Equations with Roundoff Errors in Multiplications  
and Additions

The actual system equations for additive and multiplicative round-off errors are

$$y_{mn} = f1 \left[ \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} x_{m-j,n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} y_{m-j,n-k} \right] \quad (57)$$

$$= \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} x_{m-j,n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} y_{m-j,n-k} + e_{mn}^{(d)}, \quad (58)$$

where  $y_{mn}$ ,  $x_{mn}$ ,  $b_{jk}$ , and  $a_{jk}$  are machine numbers,

$$\begin{aligned} e_{mn}^{(d)} &= \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} (\theta_{mn,jk}^{-1}) x_{m-j,n-k} \\ &\quad - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} (\varphi_{mn,jk}^{-1}) y_{m-j,n-k} \end{aligned} \quad (59)$$

$$e_{i\ell}^{(d)} = 0 \text{ for } i < 0 \text{ or } \ell < 0 ,$$

$$\theta_{mn,00} = (1 + \xi_{mn})(1 + \delta_{mn,00}) \prod_{\substack{i=0, \ell=0 \\ i+\ell \neq 0}}^{M_b, N_b} (1 + \gamma_{mn,i\ell}) , \quad (60)$$

$$\theta_{mn,jk} = (1 + \xi_{mn})(1 + \epsilon_{mn,jk}) \prod_{i=j, \ell=k}^{M_b, N_b} (1 + \gamma_{mn,i\ell}) \quad (61)$$

$j = 0, \dots, M_b,$   
 $k = 0, \dots, N_b,$   
 $j + k \neq 0,$

$$\varphi_{mn,01} = (1 + \xi_{mn})(1 + \epsilon_{mn,01}) \left( \prod_{\ell=2}^{N_a} (1 + \eta_{mn,0\ell}) \right) \left( \prod_{i=1, \ell=0}^{M_a, N_a} (1 + \eta_{mn,i\ell}) \right), \quad (62)$$

$$\varphi_{mn,0k} = (1 + \xi_{mn})(1 + \epsilon_{mn,0k}) \left( \prod_{\ell=k}^{N_a} (1 + \eta_{mn,0k}) \right) \left( \prod_{i=1, \ell=0}^{M_a, N_a} (1 + \eta_{mn,i\ell}) \right), \quad (63)$$

$k = 2, \dots, N_a$

and

$$\varphi_{mn,jk} = (1 + \xi_{mn})(1 + \epsilon_{mn,jk}) \left( \prod_{i=j, \ell=k}^{M_a, N_a} (1 + \eta_{mn,i\ell}) \right), \quad (64)$$

$k = 0, \dots, N_a$   
 $j = 1, \dots, M_a.$

For Eqs. (60) to (64), we have assumed that  $b_{jk} \neq 0$  or 1 for  $0 \leq j \leq M_b$  and  $0 \leq k \leq N_b$ , and that  $a_{jk} \neq 0$  or 1 for  $0 \leq j \leq M_a$  and  $0 \leq k \leq N_a$  except  $a_{00} = 1$ . If any of the  $b_{jk}$  or  $a_{jk}$  is 0 or 1, the multiplicative and additive roundoff errors associated with it are zero. The numbers of factors in the expressions for  $\theta_{mn,jk}$  and  $\varphi_{mn,jk}$  are respectively as follows,

$$s'_{jk} = \begin{cases} (M_b + 1)(N_b + 1) + 1, & \text{for } j = 0, k = 0, \\ (M_b - j + 1)(N_b - k + 1) + 2, & \text{otherwise,} \end{cases} \quad (65)$$

$$s'_{jk} = \begin{cases} (M_b + 1)(N_b + 1) + 1, & \text{for } j = 0, k = 0, \\ (M_b - j + 1)(N_b - k + 1) + 2, & \text{otherwise,} \end{cases} \quad (66)$$

$$\alpha'_{jk} = \begin{cases} (M_a + 1)(N_a + 1), & \text{for } j = 0, k = 1, \\ (M_a + 1)(N_a + 1) - k + 2, & \text{for } j = 0, k = 2, \dots, N_a, \\ (M_a - j + 1)(N_a - j + 1) + 2, & \text{otherwise.} \end{cases} \quad (67)$$

$$(68)$$

$$(69)$$

Notice that if some of the filter coefficients are 0 (no addition and multiplication) or 1 (no multiplication), the numbers in Eqs. (65) to (69) will be correspondingly reduced.

Since the digital filter is stable, if the number of bits  $t$  is not too small we can approximate Eq. (59) by substituting  $w_{m-j,n-k}$  for  $y_{m-j,n-k}$  (the mathematical justification is similar to the 1D case in [8]) and obtain

$$e_{mn}^{(d)} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} (\theta_{mn,jk}^{-1}) x_{m-j,n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} (\varphi_{mn,jk}^{-1}) w_{m-j,n-k}, \quad (70)$$

where  $w_{mn}$  is the ideal output.

#### Actual System Equations for Coefficient Quantizations

For coefficient quantization the actual system equations are

$$\hat{y}_{mn} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} x_{m-j,n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} \hat{y}_{m-j,n-k} + \hat{e}_{mn}^{(d)}, \quad (71)$$

where  $\hat{y}_{mn}$ ,  $b_{jk}$ ,  $a_{jk}$ , and  $x_{mn}$  are machine numbers, and

$$\hat{e}_{mn}^{(d)} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} e_{jk} \bar{b}_{jk} x_{m-j, n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} \delta_{jk} \bar{a}_{jk} \hat{y}_{m-j, n-k}, \quad (72)$$

where  $\bar{b}_{jk}$  and  $\bar{a}_{jk}$  are ideal filter coefficients,

$$|e_{jk}| < 2^{-t}, \quad \text{and}$$

$$|\delta_{jk}| < 2^{-t}.$$

Similar to Eq. (70), we can also approximate Eq. (72) by

$$\hat{e}_{mn}^{(d)} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} e_{jk} \bar{b}_{jk} x_{m-j, n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} \delta_{jk} \bar{a}_{jk} w_{m-j, n-k}, \quad (73)$$

where  $w_{mn}$  is the ideal output.

### Actual System Equations for Quantizations of Inputs and Initial Conditions

For quantized inputs and initial conditions the actual system equations are

$$\bar{y}_{mn} = \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} x_{m-j, n-k} - \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk} \bar{y}_{m-j, n-k} + \tilde{e}_{mn}^{(d)}, \quad (74)$$

where  $\bar{y}_{mn}$ ,  $b_{jk}$ ,  $a_{jk}$ , and  $x_{mn}$  are machine numbers,

$$\bar{y}_{jk} = (1 + \epsilon_{jk}) W(-j, -k), \quad (75)$$

$j = 0, \dots, M_a,$   
 $k = 0, \dots, N_a,$   
 $j + k \neq 0,$

where  $|\epsilon_{jk}| < 2^{-t}$ , and  $W(-j, -k)$  are the ideal initial conditions,

and

$$\hat{e}_{mn}^{(d)} = - \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk} (\delta_{m-j, n-k} \bar{x}_{m-j, n-k}), \quad (76)$$

where  $\bar{x}_{mn}$  is an ideal input, and

$$|\delta_{mn}| < 2^{-t}.$$

## IV.2 Behavior of the Sources of Error

Let

$$e_{mn} = y_{mn} - w_{mn}.$$

(77)

Subtracting Eq. (2) from Eq. (58), we have

$$e_{mn} = - \sum_{j=0}^{M_a} \sum_{k=0}^{N_a} a_{jk} e_{m-j, n-k} + e_{mn}^{(d)} . \quad (78)$$

$j+k \neq 0$

Eq. (78) says that the output roundoff errors  $\{e_{mn}\}$  can be interpreted as resulting from the injection of an error source  $e_{mn}^{(d)}$  into the system at the junction indicated in Figure 5(a).

Similarly, from Eqs. (2), (71), and (70), we can interpret the output errors, due to the coefficient inaccuracies or the quantizations of inputs and initial states, as resulting from error sources  $\hat{e}_{mn}^{(d)}$  or  $\tilde{e}_{mn}^{(d)}$  injected into the system at the junctions shown in Figures 5(b) and 5(c).

## IV.3 Mean Squared Error Analysis

### Basic Assumptions

As usual, we assume that the relative errors  $\delta_{mn,ij}$ ,  $\epsilon_{mn,ij}$ ,  $\gamma_{mn,ij}$ ,  $\xi_{mn,ij}$ , etc. are independent random variables and are uniformly distributed in the range  $(-2^{-t}, 2^{-t})$ . Thus they are zero mean and have a variance of  $\sigma^2 = E_o^2/3$  with  $E_o = 2^{-t}$ , and they are uncorrelated with each other or with any other signals. We also assume that the input signal  $x_{mn}$  is zero mean and wide sense stationary. Since our system is a linear spatially invariant system the output signal is also zero mean and wide sense stationary.

Mean Squared Error Estimations for Roundoff Errors

Expanding Eq. (63), we have

$$\varphi_{mn,jk} = 1 + \xi_{mn} + \epsilon_{mn,jk} + \sum_i \sum_l \eta_{mn,il} + O(2^{-2t}). \quad (79)$$

Take the first order approximation,

$$\varphi_{mn,jk}^{-1} \doteq \xi_{mn} + \epsilon_{mn,jk} + \sum_i \sum_l \eta_{mn,il}. \quad (80)$$

The right hand side of Eq. (80) has a total of  $\alpha'_{jk}$  (see Eq. (69)) independent identically distributed random variables. We then consider  $(\varphi_{mn,jk}^{-1})$  to be an independent random variable consisting of the sum of  $\alpha'_{jk}$  independent identically distributed random variables. Likewise we consider each  $(\theta_{mn,jk}^{-1})$  to be an independent random variable which is the sum of  $\beta'_{jk}$  independent identically distributed random variables.

In Eq. (70), let

$$e_{mn,jk}^{(a)} = (\varphi_{mn,jk}^{-1}) a_{jk} w_{m-j,n-k} \quad (81)$$

$$e_{mn,jk}^{(b)} = (\theta_{mn,jk}^{-1}) b_{jk} x_{m-j,n-k}. \quad (82)$$

The means of the random variables  $e_{mn,jk}^{(a)}$  and  $e_{mn,jk}^{(b)}$  are zero. Let  $\sigma_{e_{jk}}^2$  and  $\sigma_{e_{jk}}^{(b)2}$  represent their variances respectively; then,

$$\sigma_{e_{jk}}^2 = \frac{E_0^2}{3} \cdot \alpha'_{jk} \cdot \overline{(a_{jk} w_{m-j,n-k})^2}, \quad (83)$$

$$\sigma_{e_{jk}}^{(b)2} = \frac{E_0^2}{3} \cdot \beta'_{jk} \cdot \overline{(b_{jk} x_{m-j,n-k})^2}. \quad (84)$$

The bar denotes expected value. We approximate it by the following operation,

$$\overline{A^2} = \lim_{\substack{n \rightarrow \infty \\ m \rightarrow \infty}} \frac{\sum_{i=0}^m \sum_{j=0}^n A_{ij}^2}{mn} . \quad (85)$$

Considering  $e_{mn}^{(d)}$  (Eqs. (58), (59), (60), and (78)) to be composed of  $(M_b + 1) (N_b + 1)$  of the  $e_{mn,jk}^{(b)}$ 's and  $[(M_a + 1) (N_a + 1) - 1]$  of the  $e_{mn,jk}^{(a)}$ 's, then from Eqs. (83) and (84), the steady state output error is found to be

$$\sigma_e^2 = \left( \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} \sigma_{e_{jk}^{(a)}}^2 + \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_b} \sum_{k=0}^{N_b} \sigma_{e_{jk}^{(b)}}^2 \right) \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} h_{mn}^2 . \quad (86)$$

#### Mean Squared Error Estimates for Coefficient Inaccuracies

From Eqs. (71) and (73), the output error due to the quantizations of the filter coefficients can be calculated as

$$\hat{\sigma}_e^2 = \left( \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} \hat{\sigma}_{e_{jk}^{(a)}}^2 + \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_b} \sum_{k=0}^{N_b} \hat{\sigma}_{e_{jk}^{(b)}}^2 \right) \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} h_{mn}^2 , \quad (87)$$

with

$$\hat{\sigma}_{e_{jk}^{(a)}}^2 = \overline{(a_{jk} \delta_{jk} w_{m-j, n-k})^2} = \delta_{jk}^2 \overline{(a_{jk} w_{m-j, n-k})^2} , \quad (88)$$

$$\hat{\sigma}_e^2(b) = \overline{(b_{jk} \epsilon_{jk} x_{m-j, n-k})^2} = \epsilon_{jk}^2 \overline{(b_{jk} x_{m-j, n-k})^2} \quad (89)$$

where  $\delta_{jk}$  and  $\epsilon_{jk}$  are fixed numbers. For high order filters we may be able to regard  $\delta_{jk}$  and  $\epsilon_{jk}$  as random variables, and hence we can replace  $\delta_{jk}^2$  or  $\epsilon_{jk}^2$  by  $E_o^2/3$  in Eqs. (88) and (89).

#### Mean Squared Error Estimates for Quantizations of Input Signals and Initial Conditions

The output error due to the quantization of the input signal can be calculated as

$$\hat{\sigma}_e^2 = \left( \frac{E_o^2}{3} \overline{x_{mn}^2} \right) \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} g_{mn}^2 . \quad (90)$$

As for the output error due to the quantization of the initial conditions, it usually can be neglected if the impulse response dies out fast enough. The output error is governed by the following equation,

$$e_{mn} = - \sum_{j=0}^{M_a} \sum_{k=0}^{N_a} h_{mn}^{(jk)} \epsilon_{jk} W(-j, -k), \quad (91)$$

$j+k \neq 0$

where  $\epsilon_{jk}$  and  $W(-j, -k)$  are defined in Eq. (75), and  $h_{mn}^{(jk)}$  is given in Eq. (12).

The derivation of Eq. (91) is not difficult and is omitted here. Note that  $h_{mn}^{(jk)} \rightarrow 0$  and hence  $\bar{e}_{mn} \rightarrow 0$  when  $m$  and/or  $n \rightarrow \infty$ , since the digital filter is stable. It can be seen that

$$\langle \bar{e} \rangle^{K_2, K_1} \leq \sum_{j=0}^{M_a} \sum_{k=0}^{N_a} \langle h^{(jk)} \rangle^{K_2, K_1} |\epsilon_{jk} w(-j, -k)| . \quad (92)$$

The value of the right hand side dies out as  $K_2$  and  $K_1$  increase.

### Discussion

We have derived the steady state output mean squared error for each of the three sources of error. If two or more sources of error are present, the output mean squared errors due to their combined effects can be approximated by the summations of  $\sigma_e^2$  (Eq. (86)),  $\hat{\sigma}_e^2$  (Eq. (87)), and/or  $\bar{\sigma}_e^2$  (Eq. (90)).

For nonstationary or deterministic inputs we cannot obtain similar results to those in Eqs. (86), (89), and (90). As an illustration, for round-off error with deterministic inputs, we have the following equation instead of Eq. (86),

$$\begin{aligned} \sigma_{e_{mn}}^2 &= \frac{E_o^2}{3} \left[ \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk}^2 \cdot a'_{jk} \cdot \left( \sum_{\mu=0}^m \sum_{v=0}^n w_{\mu-j, v-k}^2 h_{m-\mu, n-v}^2 \right) \right. \\ &\quad \left. + \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk}^2 \cdot b'_{jk} \cdot \left( \sum_{\mu=0}^m \sum_{v=0}^n x_{\mu-j, v-k}^2 h_{m-\mu, n-v}^2 \right) \right] . \quad (93) \end{aligned}$$

### IV.4 Norm Bounds

In this section we obtain norm bounds for output errors due to the three sources of error. We still assume that the relative errors  $\gamma_{mn, jk}$ ,  $\delta_{mn, jk}$ , etc. are independent random variables uniformly distributed in  $(-2^{-t}, 2^{-t})$ . We make no assumption for the input signal.

For roundoff errors, letting  $e_{mn,jk}^{01}$  be the output error due to the error source  $e_{mn,jk}^{(a)}$ ,

$$e_{mn,jk}^{01} = \sum_{\mu=0}^m \sum_{v=0}^n (\varphi_{\mu v, jk}^{-1}) a_{jk} w_{\mu-j, v-k} h_{m-\mu, n-v}. \quad (94)$$

By lemma 1 we can obtain

$$\begin{aligned} E\{e_{jk}^{01}\}_{K_2, K_1}^2 &\leq \max_{\substack{0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi}} |D^{-1}(e^{i\omega_1}, e^{i\omega_2})|^2 \cdot \frac{E_o^2}{3} a_{jk}^2 \alpha'_{jk} \\ &\cdot {}^2 \langle w \rangle_{j,k}^{K_2, K_1} \end{aligned} \quad (95)$$

where  $E\{\cdot\}$  denotes the expected value, and we have assumed that the initial conditions of the 2D digital filters are zero. Therefore,

$$\begin{aligned} E\{e\}_{K_2, K_1}^2 &\leq \max_{\substack{0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi}} |D^{-1}(e^{i\omega_1}, e^{i\omega_2})|^2 \cdot \frac{E_o^2}{3} \\ &\cdot [ \sum_{\substack{j=0 \\ j+k \neq 0}}^{M_a} \sum_{k=0}^{N_a} a_{jk}^2 \alpha'_{jk} {}^2 \langle w \rangle_{j,k}^{K_2, K_1} + \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk}^2 \beta'_{jk} {}^2 \langle x \rangle_{j,k}^{K_2, K_1} ]. \end{aligned} \quad (96)$$

Similarly, for quantization errors of the filter coefficients, we have

$$\begin{aligned}
 E\{\hat{e}^{K_2, K_1}\} &\leq \max_{\substack{0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi}} |D^{-1}(e^{i\omega_1}, e^{i\omega_2})|^2 \cdot \left[ \sum_{j=0}^{M_a} \sum_{\substack{k=0 \\ j+k \neq 0}}^{N_a} \bar{a}_{jk}^2 b_{jk}^2 \cdot {}^2\langle w \rangle_{j,k}^{K_2, K_1} \right. \\
 &\quad \left. + \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} \bar{b}_{jk}^2 b_{jk}^2 \cdot {}^2\langle x \rangle_{j,k}^{K_2, K_1} \right]. \tag{97}
 \end{aligned}$$

For quantization errors of the input signal,

$$\begin{aligned}
 E\{\bar{e}^{K_2, K_1}\} &\leq \max_{\substack{0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi}} |G(e^{i\omega_1}, e^{i\omega_2})|^2 \cdot \frac{E_o^2}{3} \\
 &\quad \cdot \left[ \sum_{j=0}^{M_b} \sum_{k=0}^{N_b} b_{jk}^2 b'_{jk}^2 \cdot {}^2\langle x \rangle_{j,k}^{K_2, K_1} \right]. \tag{98}
 \end{aligned}$$

#### IV.5 Numerical Results

A "Decimal simulation program" has been written to simulate, decimally, all the filtering operations on a CDC 6600 computer. The program includes subroutines which simulate floating-point additions, floating-point multiplications, and quantizations. All the floating-point variables are double precision.

The following examples are among those we used to test the validity of the method in Eqs. (86), (87), (90), (96), (97), and (98). For each example with a given input signal the following quantities are calculated;

let  $\Delta = 2^{K_2, K_1}$  where  $w_{mn}$  is the ideal output sequence,

(i) RE :  $\sigma_e^2 / \Delta$ , where  $\sigma_e^2$  is the theoretical roundoff error (Eq. (86)),

(ii) RA :  $\sigma_e^2 / \Delta$ , where  $e_{mn}$  is the actual output error due to roundoffs,

(iii) RNE : Norm bound for output error due to roundoffs (Eq. (96)) divided by  $\Delta$ ,

(iv) CE :  $\hat{\sigma}_e^2$  (Eq. (87)) /  $\Delta$ ,

(v) CA :  $\hat{\sigma}_e^2 / \Delta$ , where  $\hat{e}_{mn}$  is the actual output error due to coefficient quantizations,

(vi) CNE : Norm bounds for output error due to coefficient quantizations (Eq. (97)) divided by  $\Delta$ ,

(vii) IE :  $\bar{\sigma}_e^2$  (Eq. (90)) /  $\Delta$ ,

(viii) IA :  $\bar{\sigma}_e^2 / \Delta$ , where  $\bar{e}_{mn}$  is the actual output error due to input quantizations,

(ix) INE : Norm bound for output error due to input quantizations (Eq. (98)) divided by  $\Delta$ .

(x)  $RCE = RE + CE,$

(xi)  $RCA : {}^2 \langle e^{rc} \rangle^{K_2, K_1} / \Delta,$  where  $e_{mn}^{rc}$  is the actual output error due to roundoffs and coefficient quantizations,

(xii)  $RCNE = RNE + CNE,$

(xiii)  $RCIE = RC + CE + IE,$

(xiv)  $RCIA : {}^2 \langle e^{rci} \rangle^{K_2, K_1} / \Delta,$  where  $e_{mn}^{rci}$  is the actual output error due to the combined effects of all the three sources of error,

(xv)  $RCINE = RNE + CNE + INE.$

**Example 1:** Two-dimensional Digital Filter Designed by Shanks' Rotation Method and Modified by a Planar Least Squares Inverse Algorithm ([3]).

$$\begin{aligned}
 N(z_1, z_2) = & 4.39 \times 10^{-3} + 1.317 \times 10^{-2} z_1^{-1} + 1.317 \times 10^{-2} z_1^{-2} + 4.39 \times 10^{-3} z_1^{-3} \\
 & + 1.317 \times 10^{-2} z_2^{-1} + 3.9509 \times 10^{-2} z_1^{-1} z_2^{-1} + 3.9509 \times 10^{-2} z_1^{-2} z_2^{-1} \\
 & + 1.317 \times 10^{-2} z_1^{-3} z_2^{-1} \\
 & + 1.317 \times 10^{-2} z_2^{-2} + 3.9509 \times 10^{-2} z_1^{-1} z_2^{-2} + 3.9509 \times 10^{-2} z_1^{-2} z_2^{-2} \\
 & + 1.317 \times 10^{-2} z_1^{-3} z_2^{-2} \\
 & + 4.39 \times 10^{-3} z_2^{-3} + 1.317 \times 10^{-2} z_1^{-1} z_2^{-3} + 1.317 \times 10^{-2} z_1^{-2} z_2^{-3} \\
 & + 4.39 \times 10^{-3} z_1^{-3} z_2^{-3} .
 \end{aligned}$$

$$\begin{aligned}
 D(z_1, z_2) = & 1 + 9.72193 \times 10^{-2} z_1^{-1} + 1.35846 \times 10^{-2} z_1^{-2} + 6.245431 \times 10^{-4} z_1^{-3} \\
 & + 2.105095 \times 10^{-2} z_2^{-1} - 1.785671 z_1^{-1} z_2^{-1} - 0.1398205 z_1^{-2} z_2^{-1} \\
 & - 1.197869 \times 10^{-2} z_1^{-3} z_2^{-1} \\
 & + 7.184771 \times 10^{-3} z_2^{-2} - 8.055841 \times 10^{-2} z_1^{-1} z_2^{-2} + 1.262808 z_1^{-2} z_2^{-2} \\
 & + 5.927248 \times 10^{-2} z_1^{-3} z_2^{-2} \\
 & - 7.236237 \times 10^{-4} z_2^{-3} - 5.415724 \times 10^{-3} z_1^{-1} z_2^{-3} \\
 & + 5.705888 \times 10^{-2} z_1^{-2} z_2^{-3} - 3.541561 \times 10^{-1} z_1^{-3} z_2^{-3}.
 \end{aligned}$$

The following three input signals are used:

$$2I1 : x_{jk} = \cos(j) \cos(k), j = 0, \dots, 127, \text{ and } k = 0, \dots, 127, \quad (99)$$

$$2I2 : x_{jk} = \cos(j \cdot k), j = 0, \dots, 127, \text{ and } k = 0, \dots, 127, \quad (100)$$

$$2I3 : x_{jk} = \text{noise}(j, k), j = 0, \dots, 127, \text{ and } k = 0, \dots, 127, \quad (101)$$

where noise (j, k) are generated by a random number generator.

The operations are from  $m = 0, \dots, 127$  and  $n = 0, \dots, 127$ . The impulse responses for  $1/D(z_1, z_2)$  at  $(m, n) = (0, 0)$  and  $(m, n) = (127, 127)$  are  $1.0$  and  $5.732 \times 10^{-16}$ , respectively. The number of bits for simulations is  $t = 16$ . Table 3 shows the numerical results.

E

N

Table 3

Errors	Inputs			Powers of 10.
	2I1	2I2	2I3	
RE	2.14062	2.14409	2.15345	$10^{-8}$
RA	2.76639	1.75509	1.55308	$10^{-8}$
RNE	1.47309	1.47548	1.48192	$10^{-7}$
CE	1.18103	1.19667	1.19465	$10^{-9}$
CA	2.18830	1.63675	1.57992	$10^{-9}$
CNE	8.12738	8.23503	8.22112	$10^{-9}$
IE	2.73986	8.64918	7.066	$10^{-11}$
IA	1.28770	3.15256	3.55109	$10^{-11}$
INE	0.681206	2.15043	1.75680	$10^{-9}$
RCE	2.25872	2.26376	2.27292	$10^{-8}$
RCA	2.02213	1.57048	1.40364	$10^{-8}$
RCNE	1.55437	1.55783	1.56413	$10^{-9}$
RCIE	2.26146	2.27241	2.27998	$10^{-8}$
RCIA	2.08492	1.60492	1.41122	$10^{-8}$
RCINE	1.56118	1.57934	1.58170	$10^{-7}$

Example 2: Two-Dimensional High Pass Digital Filter.

$$\begin{aligned}
 N(z_1, z_2) = & 1.2 - 3.6z_1^{-1} + 3.6z_1^{-2} - 1.2z_1^{-3} - 3.6z_2^{-1} + 10.8z_1^{-1}z_2^{-1} \\
 & - 10.08z_1^{-2}z_2^{-1} + 3.6z_1^{-3}z_2^{-1} + 3.6z_2^{-2} - 10.8z_1^{-1}z_2^{-2} \\
 & + 10.08z_1^{-2}z_2^{-2} - 3.6z_1^{-3}z_2^{-2} - 1.2z_2^{-3} + 3.6z_1^{-1}z_2^{-3} \\
 & - 3.6z_1^{-2}z_2^{-3} + 1.2z_1^{-3}z_2^{-3}.
 \end{aligned}$$

$$\begin{aligned}
 D(z_1, z_2) = & 1. -1.529578z_1^{-1} + 9.6912z_1^{-2} - 2.14664z_1^{-3} \\
 & - 1.529578z_2^{-1} + 2.339608z_1^{-1}z_2^{-1} - 1.482344z_1^{-2}z_2^{-2} \\
 & - 0.208035z_1^{-3}z_2^{-3} \\
 & + 0.96912z_2^{-2} - 1.482344z_1^{-1}z_2^{-2} + 0.939193z_1^{-2}z_2^{-2} \\
 & + 4.6081 \times 10^{-2}z_1^{-3}z_2^{-3} \\
 & - 0.214644z_2^{-3} - 3.28345z_1^{-1}z_2^{-3} - 0.208035z_1^{-2}z_2^{-3} \\
 & + 4.6081 \times 10^{-2}z_1^{-3}z_2^{-3}.
 \end{aligned}$$

The inputs used are still those in Eqs. (99), (100), and (101). Other operating conditions (number of bits, number of input and output points and etc.) are also the same as in Example 1. Table 4 gives the numerical results.

Table 4

Errors	Inputs			Power of 10
	2I1	2I2	2I3	
RE	6.70882	5.97688	6.89292	$10^{-7}$
RA	8.27063	1.54102	5.85148	$10^{-7}$
RNE	8.91590	7.94316	9.16056	$10^{-6}$
CE	5.36286	4.55883	5.56276	$10^{-8}$
CA	0.979651	1.53522	1.00613	$10^{-8}$
CNE	7.12713	6.05860	7.39280	$10^{-7}$
IE	0.429636	0.761428	1.072392	$10^{-10}$
IA	0.380303	0.322345	0.66187	$10^{-10}$
INE	1.37214	1.03698	1.46045	$10^{-10}$
RCE	7.2451	3.91965	3.95618	$10^{-7}$
RCA	8.57491	1.54024	6.69687	$10^{-7}$
RCNE	9.62861	8.54902	9.89984	$10^{-6}$
RCIE	7.2503	3.92726	3.95725	$10^{-7}$
RCIA	7.94085	1.62868	5.98533	$10^{-7}$
RCINE	9.62875	8.54913	9.89998	$10^{-6}$

Example 3: One-dimensional bandpass digital filter designed by linear programming method ([10]).

Filter Coefficients:

$$N(z) = 0.10202 - 0.3031065z^{-1} + 0.3986085z^{-2}$$

$$- 0.2786962z^{-3} + 0.0812557z^{-4}$$

$$D(z) = 1 - 2.98247z^{-1} + 3.95745z^{-2} - 2.59993z^{-3}$$

$$+ 0.758117z^{-4}.$$

Input Signals Used:

$$I1 : x_j = \cos(10j), j=0, \dots, 255,$$

$$I2 : x_j = \cos(0.1j), j=0, \dots, 255,$$

$$I3 : x_j = \cos(j), j=0, \dots, 255,$$

$$I4 : x_j = \text{noise}(j), j=0, \dots, 255,$$

$$I5 : x_j = \text{noise}(j) \cos(j), j=0, \dots, 255,$$

$$I6 : x_j = \cos(j+\text{noise}(j)), j=0, \dots, 255,$$

$$I7 : x_j = \cos(\text{noise}(j) \cdot j), j=0, \dots, 255,$$

$$I8 : x_j = \text{noise}(j) \cdot \cos(j) + \text{noise}^1(j) \cdot \sin(j), j=0, \dots, 255,$$

$$I9 : x_j = \text{noise}^2(j) \cdot \cos(j) + \text{noise}^3(j) \cdot \sin(j), j=0, \dots, 255,$$

where the signals  $\text{noise}(j)$ ,  $\text{noise}^1(j)$ ,  $\text{noise}^2(j)$ , and  $\text{noise}^3(j)$  are generated by a random number generator. They have different variances and different starting values.

The operations are from  $n = 0$  to  $n = 255$ . Table 5 lists the numerical results.

Table 5

Errors	Inputs									Powers of 10
	I1	I2	I3	I4	I5	I6	I7	I8	I9	
RE	6.73	7.05	6.51	1.64	1.60	6.15	1.73	1.60	1.61	$10^{-5}$
RA	2.25	3.00	2.05	0.75	0.52	2.25	0.71	0.52	0.91	$10^{-5}$
RNE	7.33	7.68	7.01	1.79	1.74	6.70	1.89	1.74	1.76	$10^{-4}$
CE	1.51	1.58	1.46	0.30	0.29	1.37	0.32	0.29	0.29	$10^{-5}$
CA	1.56	1.42	0.85	1.57	1.66	0.84	2.52	1.66	1.59	$10^{-5}$
CNE	16.4	17.2	15.8	3.29	3.18	14.9	3.53	3.18	3.22	$10^{-8}$
IE	1.21	1.29	1.15	0.033	0.023	1.08	0.058	0.023	0.026	$10^{-8}$
IA	0.47	0.26	0.39	0.012	0.014	0.26	0.027	0.014	0.011	$10^{-8}$
INE	13.7	14.6	13.1	0.37	0.26	12.2	0.62	0.26	0.29	$10^{-5}$
RCE	8.23	8.63	7.97	1.94	1.89	7.52	2.06	1.89	1.90	$10^{-5}$
RCA	5.51	9.60	3.38	3.23	2.97	3.02	2.52	2.97	1.72	$10^{-4}$
RCNE	8.97	9.4	8.7	2.11	2.06	8.2	2.24	2.06	2.08	$10^{-5}$
RCIE	8.23	8.63	7.97	1.94	1.89	7.52	2.06	1.89	1.90	$10^{-5}$
RCIA	6.51	8.18	2.26	2.22	2.49	2.90	2.46	2.50	2.23	$10^{-4}$
RCINE	8.97	9.41	8.7	2.11	2.06	8.2	2.24	2.06	2.08	$10^{-4}$

Table 5 - (continued)

Errors	Inputs									Powers of 10
	I1	I2	I3	I4	I5	I6	I7	I8	I9	
RE	2.51	2.63	2.43	0.61	0.60	2.29	0.65	0.60	0.60	$10^{-13}$
RA	1.36	0.90	0.79	0.47	0.25	0.74	0.32	0.25	0.54	$10^{-13}$
RNE	27.3	28.6	26.5	6.65	6.49	25.0	7.04	6.48	6.54	$10^{-13}$
CE	1.94	2.01	1.89	0.77	0.76	1.80	0.78	0.076	0.77	$10^{-14}$
CA	4.39	4.21	1.82	0.36	0.37	1.81	2.96	0.37	0.36	$10^{-14}$
CNE	21.1	21.9	20.6	8.41	8.31	19.7	8.52	8.31	8.35	$10^{-14}$
IE	4.52	4.80	4.33	0.123	0.089	4.01	0.22	0.087	0.095	$10^{-17}$
IA	1.84	1.36	1.98	0.056	0.039	1.30	0.084	0.039	0.054	$10^{-17}$
INE	51.4	54.6	49.0	1.40	0.98	45.5	0.25	0.98	1.08	$10^{-17}$
RCE	2.70	2.83	2.61	0.69	0.67	2.47	0.72	0.67	0.68	$10^{-13}$
RCA	1.22	0.94	1.32	0.47	0.70	0.86	0.40	0.70	0.48	$10^{-13}$
RCNE	29.4	30.8	28.5	7.50	7.32	26.9	7.89	7.32	7.37	$10^{-13}$
RCIE	2.70	2.83	2.62	0.69	0.67	2.47	0.72	0.67	0.68	$10^{-13}$
RCIA	1.45	1.98	1.05	0.34	0.61	0.64	0.70	0.61	0.63	$10^{-13}$
RCINE	29.4	30.8	28.5	7.50	7.32	27.0	7.89	7.32	7.37	$10^{-13}$

## V. DISCUSSION AND CONCLUSION

### V.1 Discussion

We have a unified approach for dealing with uncorrelated errors in both floating-point and fixed-point two-dimensional digital filters. For both kinds of filters we have adopted the same method to derive formulas for estimating the output mean squared errors and output norm error bounds. (Note that mean squared errors and norm error bounds together should furnish us enough information to determine how many bits are needed for a digital filter to have certain desired performance.)

Eqs. (34), (35), (86), (87) and (90) require the calculations of the unit impulse responses ( $\sum_m \sum_n h_{mn}^2$  and  $\sum_m \sum_n g_{mn}^2$ ). They could be replaced by the frequency evaluations,

$$\sum_{m=0}^{\infty} \sum_{n=0}^{\infty} h_{mn}^2 = \frac{1}{(2\pi i)^2} \oint_{|z_1|=1} \oint_{|z_2|=1} \frac{1}{D(z_1, z_2) D(1/z_1, 1/z_2)} \frac{dz_1}{z_1} \frac{dz_2}{z_2} \quad (102)$$

and

$$\sum_{m=0}^{\infty} \sum_{n=0}^{\infty} g_{mn}^2 = \frac{1}{(2\pi i)^2} \oint_{|z_1|=1} \oint_{|z_2|=1} G(z_1, z_2) G(\frac{1}{z_1}, \frac{1}{z_2}) \frac{dz_1}{z_1} \frac{dz_2}{z_2}. \quad (103)$$

Closed form solutions of Eqs. (102) and (103) for 2D recursive digital filters are usually out of reach. Approximations are possible and one way of doing it is via FFT.

For digital filters with high gain and narrow passband area (these filters are difficult to implement), the present method of estimating the mean squared errors is difficult, since the impulse responses die out

slowly, and the approximations of Eqs. (102) and (103) also require very fine step sizes. However, in many important applications ([1]) of 2D signal processing we usually require that the results of the recursive filtering be roughly independent of the initial conditions since they are usually unknown. Thus, we require that  $h_{mn}$  and hence  $g_{mn}$  die out fast enough. This means that the calculations of  $\sum_m \sum_n h_{mn}^2$  and  $\sum_m \sum_n g_{mn}^2$  can be cut at a reasonably small length of  $m$  and  $n$ . So, for some practical 2D recursive digital filters, the present method should serve as an effective way of estimating the output mean squared errors.

The results in Chapters III and IV can be applied to one- and multi-dimensional digital filters, and similar approaches can be adapted to analyzing the error properties of filters realized in different forms. However, for many one-dimensional digital filters, the frequency domain evaluations

for  $\sum_{n=0}^{\infty} h_n^2$ ,  $w_n^2$ , and etc. are easier.

## V.2 Conclusion

Block diagram representations of a two-dimensional digital filter have been introduced. A systematic treatment of uncorrelated errors for both floating-point and fixed-point 2D digital filters is presented. The analytic results include output norm error bounds (Eqs. (40), (47), (48), (49), (96), (97), and (98)) and output mean squared error estimations (Eqs. (34), (35), (36), (86), (87), and (90)). The numerical experiments have shown that the estimated errors are within an order of magnitude of the actual errors.

## APPENDIX I

### (i) 2D Z-transform

The 2D Z-transform  $X(z_1, z_2)$  of the 2D sequence  $\{x_{mn}\}_{m=0, n=0}^{\infty, \infty}$  is defined by the double summation as:

$$Z\{x_{mn}\} = X(z_1, z_2) = \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} x_{mn} z_1^{-m} z_2^{-n} \quad (A.1)$$

where  $z_1$  and  $z_2$  are complex variables. If the sequence  $\{x_{mn}\}$  satisfies the properties:

- (a)  $|x_{mn}| < \infty$  for all finite  $m$  and  $n$ ,
- (b)  $|x_{mn}| < K R_1^m R_2^n$ , for all  $n > \hat{N}$  or  $m > \hat{M}$ ,

where  $R_1$ ,  $R_2$ ,  $\hat{N}$ ,  $\hat{M}$ , and  $K$  are constants, the summation (A.1) converges absolutely. The region of the convergence of the series (A.1) is

$$D = \{(z_1, z_2) : |z_1| > R_1 \text{ and } |z_2| > R_2\}.$$

The proof of this result follows easily by considering the summation (A.1) in several parts, i.e. for (i)  $m < \hat{M}$ ,  $n < \hat{N}$ , (ii)  $m > \hat{M}$ ,  $n < \hat{N}$ , (iii)  $m < \hat{M}$ ,  $n > \hat{N}$ , and (iv)  $m > \hat{M}$ ,  $n > \hat{N}$ . It may be emphasized that the Series (A.1) is a doubly infinite series because of the two indices  $m$  and  $n$ . There are several ways of summing a series of this nature, and it is absolutely convergent if at least one arrangement for its summation converges absolutely. Further, any rearrangement of an absolutely convergent series leads to an absolutely convergent series, and the sum is the same for all arrangements.

The inversion formula for the above transform is given by

$$x_{jk} = \frac{1}{(2\pi i)^2} \oint_{c_1} \oint_{c_2} X(z_1, z_2) z_1^{j-1} z_2^{k-1} dz_1 dz_2, \quad (\text{A.2})$$

where the paths of integration  $c_1$  and  $c_2$  are within the region of the convergence of the Series (A.1). In particular,  $c_1$  is the contour  $|z_1| = R_1^* > R_1$ , and  $c_2$  is the contour  $|z_2| = R_2^* > R_2$ . This formula follows by substituting for  $X(z_1, z_2)$  in the right-hand side of (A.2), which yields

$$\oint_{c_1} \oint_{c_2} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} x_{mn} z_1^{j-m-1} z_2^{k-n-1} dz_1 dz_2. \quad (\text{A.3})$$

The interchange of summations and integration gives

$$\sum_{m=0}^{\infty} \sum_{n=0}^{\infty} x_{mn} \oint_{c_1} \oint_{c_2} z_1^{j-m-1} z_2^{k-n-1} dz_1 dz_2. \quad (\text{A.4})$$

The absolute and uniform convergence of the series for  $X(z_1, z_2)$  justifies this interchange. By the Cauchy Integral Theorem of two variables (Kaplan [14]), if the paths of integration  $c_1$  and  $c_2$  lie in the region of convergence of the series, as chosen above, it follows that

$$\oint_{c_1} \oint_{c_2} z_1^{j-m-1} z_2^{k-n-1} dz_1 dz_2 = \begin{cases} 0, & j \neq m \text{ or } k \neq n, \\ (2\pi i)^2, & j=m \text{ and } k=n. \end{cases} \quad (\text{A.5})$$

There is another expression for the inverse transform given by

$$x_{jk} = \frac{1}{j! k!} \left[ \frac{\partial^{j+k}}{(\partial z_1^{-1})^j (\partial z_2^{-1})^k} X(z_1, z_2) \right]_{z_1=\infty, z_2=\infty}. \quad (\text{A.6})$$

The expression (A.6) follows from expanding the function  $X(z_1, z_2)$  in the neighborhood of  $z_1^{-1} = 0 = z_2^{-1}$ . In the case  $X(z_1, z_2)$  is a given rational

function of  $z_1^{-1}$  and  $z_2^{-1}$ ,  $x_{jk}$  may be evaluated by determining the Series (A.1) by long division. The relationship (A.1) between  $X(z_1, z_2)$  and  $\{x_{mn}\}$  is designated by the notation  $\{x_{mn}\} \Leftrightarrow X(z_1, z_2)$ .

Many properties of the one-dimensional Z-transform are still true when they are extended suitably to the 2D Z-transform. The following properties are needed in the development of the present paper. The proofs are omitted since they follow simply from the definition of the 2D Z-transform.

(a) Linearity:

$$Z\{ax_{mn} + by_{mn}\} = aZ\{x_{mn}\} + bZ\{y_{mn}\} \quad (\text{A.7})$$

where  $a$  and  $b$  are constants, and  $\{x_{mn}\}$ ,  $\{y_{mn}\}$  are 2D sequences.

(b) Shifting:

$$\begin{aligned} Z\{x_{m+\hat{M}, n+\hat{N}}\} &= z_1^{\hat{M}} z_2^{\hat{N}} Z\{x_{mn}\} \\ &- \sum_{j=0}^{\hat{M}} \sum_{k=0}^{\hat{N}} x_{jk} z_1^{\hat{M}-j} z_2^{\hat{N}-k} \\ &\quad j+k \neq \hat{M}+\hat{N} \end{aligned} \quad (\text{A.8})$$

where  $x_{jk} = 0$ , for  $j < 0$  or  $k < 0$ ,  $j$  and  $k$  not equal to zero.

(c) Convolution in space domain:

Let  $W(z_1, z_2) \Leftrightarrow \{w_{mn}\}$ ,  $G(z_1, z_2) \Leftrightarrow \{g_{jk}\}$  and  $X(z_1, z_2) \Leftrightarrow \{x_{mn}\}$ .

If  $W(z_1, z_2) = G(z_1, z_2) X(z_1, z_2)$ , then

$$w_{mn} = \sum_{j=0}^m \sum_{k=0}^n g_{jk} x_{m-j, n-k} = \sum_{j=0}^m \sum_{k=0}^n g_{m-j, n-k} x_{jk}. \quad (\text{A.9})$$

(d) Convolution in frequency domain:

Let  $U(z_1, z_2) \leftrightarrow \{U_{mn}\}$ ,  $X(z_1, z_2) \leftrightarrow \{X_{mn}\}$ , and  $Y(z_1, z_2) \leftrightarrow \{Y_{mn}\}$ .

If  $\{X_{mn} Y_{mn}\} = \{U_{mn}\}$ , then

$$U(z_1, z_2) = \frac{1}{(2\pi i)^2} \oint_{c_1} \oint_{c_2} X\left(\frac{z_1}{v_1}, \frac{z_2}{v_2}\right) Y(v_1, v_2) v_1^{-1} v_2^{-1} dv_1 dv_2 \quad (\text{A.10})$$

where the contours are obtained by the simple generalization of the one-dimensional case as in Kuo [15].

A special case of the above result is given by the following equality:

$$\sum_{m=0}^{\infty} \sum_{n=0}^{\infty} X_{mn}^2 = \frac{1}{(2\pi i)^2} \oint_{|v_1|=1} \oint_{|v_2|=1} X\left(\frac{1}{v_1}, \frac{1}{v_2}\right) X(v_1, v_2) v_1^{-1} v_2^{-1} dv_1 dv_2 \quad (\text{A.11})$$

where  $X(z_1, z_2)$  is convergent for  $|z_1| \geq 1$ ,  $|z_2| \geq 1$ .

### (ii) Proof of Lemma 1

First, we show that

$$\sum_{m=0}^{K_2} \sum_{n=0}^{K_1} |\hat{f}_{mn}|^2 = \frac{1}{4\pi^2} \int_0^{2\pi} \int_0^{2\pi} |F(\omega_1, \omega_2)|^2 d\omega_2 d\omega_1 \quad (\text{A.12})$$

where

$$F(\omega_1, \omega_2) = \sum_{m=0}^{K_2} \sum_{n=0}^{K_1} \hat{f}_{mn} e^{-im\omega_1} e^{-in\omega_2} \quad (\text{A.13})$$

and  $\hat{f}_{mn} = \begin{cases} f_{mn} & , \quad m \leq M \text{ and } n \leq N, \\ 0 & , \quad \text{otherwise.} \end{cases}$

It is known that

$$\text{if } \hat{y}_n = y_n ; \quad n \leq N, \\ = 0 ; \quad n > N,$$

$$\text{and } f(\omega) = \sum_{n=0}^N \hat{y}_n e^{-in\omega}, \quad (\text{A14})$$

then

$$\sum_{n=0}^{\infty} |\hat{y}_n|^2 = \frac{1}{2\pi} \int_0^{2\pi} |f(\omega)|^2 d\omega, \quad (\text{A15})$$

where  $\{y_n\}$  can be a complex sequence.

Rewrite (A13) as

$$F(\omega_1, \omega_2) = \sum_{m=0}^{K_2} \left( \sum_{n=0}^{K_1} \hat{f}_{mn} e^{-in\omega_2} \right) e^{-im\omega_1}. \quad (\text{A16})$$

By (L4) it follows that

$$\sum_{m=0}^{\infty} \left| \left( \sum_{n=0}^{K_1} \hat{f}_{mn} e^{-in\omega_2} \right) \right|^2 = \frac{1}{2\pi} \int_0^{2\pi} |F(\omega_1, \omega_2)|^2 d\omega_1, \quad (\text{A17})$$

and on integrating with respect to  $\omega_2$ , one obtains:

$$\frac{1}{2\pi} \int_0^{2\pi} \sum_{m=0}^{\infty} \left| \left( \sum_{n=0}^{K_1} \hat{f}_{mn} e^{in\omega_2} \right) \right|^2 d\omega_2 = \frac{1}{2\pi} \int_0^{2\pi} \frac{1}{2\pi} \int_0^{2\pi} |F(\omega_1, \omega_2)|^2 d\omega_1 d\omega_2$$

or

$$\begin{aligned} \sum_{m=0}^{\infty} \left[ \frac{1}{2\pi} \int_0^{2\pi} \left| \sum_{n=0}^{\infty} \hat{f}_{mn} e^{-in\omega_2} \right|^2 d\omega_2 \right] \\ = \frac{1}{4\pi^2} \int_0^{2\pi} \int_0^{2\pi} |F(\omega_1, \omega_2)|^2 d\omega_1 d\omega_2. \end{aligned} \quad (\text{A18})$$

Again, by (15) one gets (A12). Now, by (A12),

$$\begin{aligned}
 \sum_{m=0}^{K_2} \sum_{n=0}^{K_1} |f_{mn}|^2 &= \frac{1}{4\pi^2} \int_0^{2\pi} \int_0^{2\pi} \left| \sum_{m=0}^{K_2} \sum_{n=0}^{K_1} e^{-im\omega_1} e^{-in\omega_2} \sum_{k=0}^m \sum_{l=0}^n C_{m-k, n-l} g_{kl} \right|^2 \\
 &\quad d\omega_2 d\omega_1, \\
 &= \frac{1}{4\pi^2} \int_0^{2\pi} \int_0^{2\pi} \left| \sum_{m=0}^{K_2} \sum_{n=0}^{K_1} e^{-im\omega_1} e^{-in\omega_2} \sum_{k=0}^m \sum_{l=0}^n C_{m-k, n-l} \hat{g}_{kl} \right|^2 \\
 &\quad d\omega_2 d\omega_1, \tag{A19}
 \end{aligned}$$

in which

$$\begin{aligned}
 \hat{g}_{kl} &= g_{kl}, \text{ for } k \leq M, \text{ and } l \leq N \tag{A20} \\
 &= 0, \quad \text{otherwise.}
 \end{aligned}$$

Further

$$\begin{aligned}
 \sum_{m=0}^{K_2} \sum_{n=0}^{K_1} |f_{mn}|^2 &\leq \frac{1}{4\pi^2} \int_0^{2\pi} \int_0^{2\pi} \left| \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} e^{-im\omega_1} e^{-in\omega_2} \sum_{k=0}^m \sum_{l=0}^n C_{m-k, n-l} \right. \\
 &\quad \left. \hat{g}_{kl} \right|^2 d\omega_2 d\omega_1, \tag{A21}
 \end{aligned}$$

(After reordering and factoring)

$$\begin{aligned}
 &\leq \frac{1}{4\pi^2} \int_0^{2\pi} \int_0^{2\pi} \left| \sum_{k=0}^{\infty} \sum_{l=0}^{\infty} C_{kl} e^{-ik\omega_1} e^{-il\omega_2} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} e^{-im\omega_1} e^{-in\omega_2} \right. \\
 &\quad \left. \hat{g}_{mn} \right|^2 d\omega_2 d\omega_1, \tag{A22}
 \end{aligned}$$

$$\leq \max_{\substack{0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi}} \left| \sum_{k=0}^{\infty} \sum_{l=0}^{\infty} C_{kl} e^{-ik\omega_1} e^{-il\omega_2} \right|^2.$$

$$\frac{1}{4\pi^2} \int_0^{2\pi} \int_0^{2\pi} \left| \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} e^{-im\omega_1} e^{-in\omega_2} \hat{g}_{mn} \right|^2 d\omega_2 d\omega_1 \quad (\text{A23})$$

$$= \max_{\begin{array}{l} 0 \leq \omega_1 \leq 2\pi \\ 0 \leq \omega_2 \leq 2\pi \end{array}} \left| \sum_{k=0}^{\infty} \sum_{l=0}^{\infty} C_{kl} e^{-ik\omega_1} e^{-il\omega_2} \right|^2 \sum_{m=0}^{K_2} \sum_{n=0}^{K_1} |g_{mn}|^2 \quad (\text{A24})$$

which proves the Lemma. The present lemma is a generalization of a similar lemma in one-dimension by Sandberg [4].

APPENDIX II  
PROGRAM LISTINGS

A

SUBROUTINE DF2I (IESTRP, ERMST, ERMSTRU, HY, EOSQRE, MH, H, HX, GMX, HMX,  
 \*ERMSTB, ERMSTB0)

C  
 C  
 C PURPOSE :  
 TO CALCULATE (1) THE MEAN SQUARED ERROR ESTIMATIONS AND (2) THE  
 NORM ERROR BOUNDS FOR ALL SOURCES OF ERROR IN TWO-DIMENSIONAL  
 DIGITAL FILTERS EMPLOYING FLOATING-POINT ARITHMETIC.  
 C  
 C  
 ATTENTION :  
 WITH SOME CHANGES, THIS SUBROUTINE CAN BE EASILY MODIFIED  
 TO DO THE SAME JOB FOR TWO-DIMENSIONAL DIGITAL FILTERS  
 EMPLOYING FIXED-POINT ARITHMETIC.  
 C  
 C  
 SUBROUTINES NEEDED :  
 FLTGR, WNTZU, SHFT.  
 C  
 C  
 INPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
 IESTRP, HY, EOSURE, MH, H, GMX, HMX, A, B, X, Y, NA, MB, NB,  
 MM, NN, NSTURE.  
 C  
 C  
 OUTPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
 ERMST, ERMSTRO, ERMSTB, ERMSTB0, HY, MH, H, HX, Y.  
 C  
 C  
 DESCRIPTIONS OF INPUT AND OUTPUT ARGUMENTS :  
 C  
 C  
 IESTRP=1 : NO CALCULATIONS FOR MH, H, AND HX.  
 IESTRP=0 : NO CALCULATIONS FOR MH AND H.  
 IESTRP=-1 : CALCULATIONS FOR MH, H, AND HX.  
 ERMST(I) : TO STORE THE ESTIMATED OUTPUT MEAN SQUARED ERROR.  
 HY : THE OUTPUT SQUARE SUM.  
 ERMSTRU(I) : ERMST(I)/HY.  
 EOSURE : EO\*EU, WHERE EU IS THE QUANTIZATION STEP SIZE.  
 MH : THE IMPULSE RESPONSE SQUARE SUM FOR THE DENOMINATOR FILTER.  
 H : THE IMPULSE RESPONSE SQUARE SUM FOR THE WHOLE FILTER.  
 HX : THE INPUT SQUARE SUM.  
 GMX : THE SQUARED VALUE OF THE MAXIMUM AMPLITUDE FREQUENCY RESPONSE  
 FOR THE WHOLE FILTER.  
 HMX : THE SQUARED VALUE OF THE MAXIMUM AMPLITUDE FREQUENCY RESPONSE  
 FOR THE DENOMINATOR FILTER.  
 ERMSTB(I) : TO STORE THE ESTIMATED NORM ERROR BOUND.  
 ERMSTB0(I) : ERMSTB(I)/HY.  
 ((A(I,J), I=1,...,MA), J=1,...,NA), ((B(I,J), I=1,...,MB), J=1,...,NB) :  
 STORING THE TWO-DIMENSIONAL DIGITAL FILTER COEFFICIENTS.  
 A FOR DENOMINATOR COEFFICIENTS.  
 B FOR NUMERATOR COEFFICIENTS.  
 MM, NN : SPATIAL RANGE OF FILTERING OPERATIONS.  
 TOTALLY (MM\*NN) POINTS.  
 (((X(I,J), Y(I,J)), J=1,...,NN), I=1,...,MM) :  
 INPUT AND OUTPUT POINTS OF THE DIGITAL FILTER.  
 NSTURE : NN\*2, THE NUMBER OF COMPUTER WORDS TRANSFERRED BACK AND  
 FORTH BETWEEN DISK AND CENTRAL MEMORY.  
 C  
 C  
 C  
 C  
 C

```

COMMON/DFC11/A(4,4),B(4,4),Y(4,128),A(4,128)
COMMON/DFC12/MA,NA,MB,JH,MM,NN,INSTURE
COMMON/DFC17/ERROR
COMMON/SHT1/STORE(128)
DIMENSION YMA(4,4),YMB(4,4),ALPHA(4,4),BETA(4,4),QEA(4,4),QEB(4,4)
*,ERMST(9),ERMSTRO(9),JEB(4,4),ERMSTB(5),ERMSTBO(5)
LOGICAL IAUXIL,INDXL
DOUBLE PRECISION A,B,Y,X,YMA,YMB,V,MY,HH,ALPHA,BETA,QEA,QEB,HD,HR,
*STORE,H,EUSQRE,AUX1,AUX2,FREF,HA,HB,NM,HBON4,HR

C
CALL IUP(3HREW,1)
CALL IUP(3HREW,2)
IF(IESTRP) 141,141,142
121 DO 24 I=1,MA
DO126 J=1,NN
126 Y(I,J)=U,U
DO 24 J=1,NN
24 YMA(I,J)=U,U
DO 124 I=1,MB
DO 27 J=1,NN
27 X(I,J)=U,U
DO124 J=1,NN
124 YMB(I,J)=U,U

C
C
IAUXIL=.F.
HX=0,U
H=0,0
INU=-1
INDGT=1
IAUXIL=.F.

C
647 DO 62 M=1,MM
CALL SHT (IND,M)
DO 62 N=1,NN
Y(MA,N)=U,U
GO TO (644,700),INDGT
C
700 DO964 J=1,NN
LJ=N+1
IF(LJ,LT,1) GO TO964
DO 64 I=1,MB
LI=MB+I+1
V=X(LI,LJ)*B(I,J)
Y(MA,N)=Y(MA,N)+V
GO TO (64,674),INDGT
674 YMB(I,J)=YMB(I,J)+V*V
64 CONTINUE
954 CONTINUE
C
GO TO 645
C
664 IF(IAUXIL) GO TO 645
IF(IND) 679,669,679
679 Y(MA,N)=1,U
GO TO 554
669 IF(M,GT,(MB+1)) GO TO 659
X(MB,N)=U,U
IF(M,EQ,1,ANU,N,EQ,1) X(MB,N)=1,U
GO TO 700
659 IAUXIL=.T.

C

```

```

665 0J96E J=1,NA
LJ=N-J+1
IF(LJ.LT.1) GO TO 966
IA=1
IF(J,EV,1) IA=2
DO 66 I=MA,NA
LI=MA=I+1
V=Y(L1,LJ)*A(I,J)
Y(MA,N)=Y(MA,V)=V
GO TO (60,670),INDGT
670 YMA(I,J)=YMA(I,J)+V*V
66 CONTINUE
656 CONTINUE
C
H=H+Y(-A,N)*Y(MA,N)
IF(INDXL) HX=HA+A(MA,V)*C(MA,V)
52 CONTINUE
C
C
IF(IND) 701,646,702
701 HM=H
PRINT 1773, HM
1773 FORMAT(1A//1A,*THE IMPULSE RESPONSE SCORE SUMS OF THE*,*
** DENOMINATOR FILTER * *,017,10)
H=0.0D0
IF(IERROR,EQ,1) INDAL=.T.
IND=1
INDGT=2
DO 16 I=1,MA
DO 16 J=1,NN
16 Y(I,J)=0.
C
C
GO BACK TO FIND THE OUTPUTS WITH INPUTS *
GO TO 647
C
162 HY=H
C
C
DO 58 I=1,MA
DO 57 J=1,NN
57 STORE(J)=Y(I,J)
58 CALL INP(ZHWB,Z,STORE,STORE)
C
C
PREPARE TO GO BACK TO FIND THE IMPULSE RESPONSE FOR THE
WHOLE FILTER
C
C
IND=0
INDGT=1
DO 14 I=1,MA
DO 14 J=1,NN
14 X(I,J)=0.0D0
H=0.0D0
INDXL=.F.
DO 15 I=1,MA
DO 15 J=1,NN
15 Y(I,J)=0.0D0
IAUX1L=.F.
GO TO 547
C
SET UP VARIOUS PARAMETER VALUES FOR ERROR ESTIMATIONS.
C
C
C*****
```

```

C      THE FOLLOWING STATEMENTS SHOULD BE PROPERLY ADJUSTED WHEN ONE OR
C      MORE OF THE FILTER COEFFICIENTS IS ZERO OR ONE.
C*****
C 840 DO 824 I=1,MB
     DO 824 J=1,NA
       IF(I.EQ.1.AND.J.EQ.1) BETA(I,J)=(MB*NB)
       IF(I.NE.1.OR.J.NE.1) BETA(I,J)=((MB-I)*(NA-J)+1)
 824 CONTINUE
     DO 26 I=1,MA
     DO 26 J=1,NA
       IF(I.EQ.1.AND.J.EQ.2) ALPHA(I,J)=MA*NA
       IF(I.EQ.1.AND.J.EQ.2) ALPHA(I,J)=(MA*NA-J+2)
       IF(I.EQ.1.AND.J.EQ.1) ALPHA(I,J)=0.
       IF(I.NE.1) ALPHA(I,J)=(MA-I)*(NA-J)+2)
 26 CONTINUE
C*****
     DO 224 I=1,MB
     DO 224 J=1,NB
 224 NEBO(I,J)=YMB(I,J)/3.0D0*BETA(I,J)
     DO 226 I=1,MA
     DO 226 J=1,NA
 226 NEA(I,J)=YMA(I,J)/3.0D0*ALPHA(I,J)
 192 HR=0.
     DO 228 I=1,MA
     DO 228 J=1,NA
 228 HR=HR+NEA(I,J)
     HBRNM=0.0D0
     DO 230 I=1,MB
     DO 230 J=1,NB
 230 HBNM=HBNM+WEBO(I,J)
     MMNN=MMNN
     HD=0.
     HBNM=0.0D0
     DO 771 I=1,MB
     DO 771 J=1,NA
       AUX1=B(I,J)
       CALL FLTGH(AUX1,FREE,RADIUS,T0,T0,AUX2)
       AUX1=(AUX1-AUX2)/AUX2
       HBNM=HBNM+YMB(I,J)*AUX1*AUX1
 771 DO 772 I=1,MA
     DO 772 J=1,NA
       AUX1=A(I,J)
       CALL FLTGH(AUX1,FREE,RADIUS,T0,T0,AUX2)
       AUX1=(AUX1-AUX2)/AUX2
       HD=HD+YMA(I,J)*AUX1*AUX1
 772 IF(IESTRP.LE.0) PRINT 1774,M
 1774 FORMAT(1X,*THE IMPULSE RESPONSE SPECTRUM OF THE*,
** WHOLE FILTER *  *,12X,017.10//)

C      ROUND OFF ERRORS ESTIMATION
C
C      ERMST(1)=(HR+HBRNM)*MH*E1*SWRE
C      ERMSTHU(1)=ERMST(1)/MH
C      ERMST(1)=ERMST(1)/MMNN

C      ESTIMATION OF COEFFICIENT QUANTIZATION ERRORS
C
C      ERMST(2)=(HD+HBNM)*MH
C      ERMSTHU(2)=ERMST(2)/MH
C      ERMST(2)=ERMST(2)/MMNN

C      ESTIMATION OF INPUT QUANTIZATION ERRORS

```

```

C      ERMST(1)=MX*H*EUSQRE/3.0F
C      ERMSTRO(3)=ERMST(3)/HY
C      ERMST(3)=ERMST(3)/MMNN

C      ERMST(4)=ERMST(1)+ERMST(2)
C      ERMSTRO(4)=ERMSTRO(1)+ERMSTRO(2)
C      ERMST(5)=ERMST(4)+ERMST(3)
C      ERMSTRO(5)=ERMSTRO(4)+ERMSTRO(3)

C
C      ESTIMATION OF NORM ERROR BOUNDS
C
C      ERMSTH(1)=(HR+HBRNM)*HUX*EUSQRE
C      ERMSTH(2)=(HU+HHNM)*HMX
C      ERMSTH(3)=HX*GMA*EUSQRE/3.0F
C      ERMSTHO(1)=ERMSTH(1)/HY
C      ERMSTHO(2)=ERMSTH(2)/HY
C      ERMSTHO(3)=ERMSTH(3)/HY
C      ERMSTHO(1)=ERMSTH(1)/MMNN
C      ERMSTHO(2)=ERMSTH(2)/MMNN
C      ERMSTHO(3)=ERMSTH(3)/MMNN
C      ERMSTHO(4)=ERMSTH(1)+ERMSTH(2)
C      ERMSTHO(5)=ERMSTH(4)+ERMSTH(3)
C      ERMSTHO(6)=ERMSTH(1)+ERMSTH(2)
C      ERMSTHO(7)=ERMSTH(4)+ERMSTH(5)+ERMSTH(3)

C      RETURN
C      END

```

```

SUBROUTINE SHFT(ISTOR,M)
C
C PURPOSE :
C   AN AUXILIARY SUBROUTINE FOR SUBROUTINE DFCI.
C
COMMON/DFCI/I1/A(4,4),B(4,4),Y(4,128),X(4,128)
COMMON/DFCI/I2/MA,MB,NR,MM,NN,NSTORE
COMMON/SHFT1/STORE(128)
DOUBLE X,STORE,Y,A,B
C
IF(ISTOR) 101,104,100
100 DO 1 I=2,MB
  DO 1 J=1,NN
    1 X(I,J)=A(I,J)
    CALL IUP(1,STORE,STORE)
    DO 2 J=1,NN
      2 X(MB,J)=STORE(J)
    GO TO 101
104 IF(M.GT.(MB+1)) GO TO 101
  DO 6 I=1,MB
    6 X(I-1,I)=A(I,I)
  101 IF(M.LE.MA) GO TO 102
    DO 3 J=1,NN
      3 STORE(J)=Y(1,J)
      IF(ISTOR) 102,102,110
110 CALL IUP(1,STORE,STORE)
102 DO 4 I=2,MA
    DO 4 J=1,NN
      4 Y(I-1,J)=Y(I,J)
  RETURN
END

```

SUBROUTINE DF2D (ERMAX, ERMS, ERMSRU, HY)

PURPOSE :  
TO SIMULATE THE OPERATIONS OF TWO-DIMENSIONAL DIGITAL FILTER EMPLOYING FLOATING POINT ARITHMETIC.

NOTE :  
THIS SUBROUTINE CAN BE MODIFIED TO BECOME A MUCH SIMPLER VERSION WHICH SIMULATES THE OPERATIONS OF TWO-DIMENSIONAL DIGITAL FILTER EMPLOYING FIXED-POINT ARITHMETIC.

SUBROUTINES NEEDED :  
FLTGA, FLTGR, FLTGM, QVTZD, SHFTDR.

INPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
HY, A, B, Y, A, MA, NA, MB, NB, MM, NN, NSTORE.  
EOH, EOI, EUVER1, EUVER2, UL2, IS.

OUTPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
ERMAX, ERMS, ERMSRU, YNT.

DESCRIPTIONS OF INPUT AND OUTPUT ARGUMENTS :  
HY, A, B, Y, A, MA, NA, MB, NB, MM, NN, NSTORE : PLEASE SEE SUBROUTINE DF2I.  
EOH, EOI, EUVER1, EUVER2, UL2, IS : PLEASE SEE SUBROUTINE FLTGA.  
INUQHL=1 : SIMULATIONS INCLUDING ROUND-OFFS.  
INUQCL=1 : SIMULATIONS INCLUDING COEFFICIENT QUANTIZATIONS.  
INUQIL=1 : SIMULATIONS INCLUDING INPUT QUANTIZATIONS.  
ERMAX : THE MAXIMUM ACTUAL ERROR.  
ERMS : THE ACTUAL MEAN SQUARED ERROR.  
ERMSRU : ERMS/HY.  
((YNT(I,J), J=1,...,NN), I=1,...,MM) : THE ACTUAL OUTPUTS OF THE DIGITAL FILTER.

COMMON/QVTZD/E0, EOH, EOI, EUVER1, EUVER2  
COMMON/FLTGR1/UL2, IS  
COMMON/SHTT1/SURE(128)  
COMMON/DF2I1/A(4,4), B(4,4), Y(4,128), X(4,128)  
COMMON/DF2I2/MA, MB, NB, MM, NN, NSTORE  
COMMON/FLTGM1/INUQHL/DF2DH1/INUQCL/INUQIL  
COMMON/JFCUR4/VNYNT(4,128), VNX(4,128), KAYNT(4,128), KAX(4,128)  
DIMENSION AA(4,4), BB(4,4), KA(4,4), KB(4,4)  
LOGICAL INUQHL, INUQCL, INUQIL, KAUXTL  
DOUBLE PRECISION A, B, Y, X, YNT, AA, BB, E0, EOH, UL2, HY, FREE, VNYNT, VNX,  
NSTORE, AJA1, AUX2, AUAY, EUVI, EUVER1, EUVER2

CALL IOP(3HRE#91)  
CALL IOP(3HHE#92)  
ERMS=0.  
ERMAX=0.

```

KAUX1=L=I+1,JCL
DO 32 I=1,MA
DO 32 J=1,NA
AJA1=A(I,J)
32 CALL FLTGR (AJA1,AA(I,J),KA(I,J),KAUX1,F.,FREE)
DO 30 I=1,MB
DO 30 J=1,NN
AJA1=B(I,J)
30 CALL FLTGR (AJA1,BB(I,J),KB(I,J),KAUX1,F.,FREE)

C
C
C
DO 24 I=1,1A
DO 24 J=1,NN
VNYNT(I,J)=0.00
24 KAYNT(I,J)=0
DO 26 I=1,MB
DO 26 J=1,NN
VNA(I,J)=0.00
26 KA(X(I,J))=0

C
DO 62 I=1,MM
CALL SIFTDH
DO 62 J=1,NN
AJAY=0.00
KAUY=0.00

C
DO 64 J=1,MB
LI=MH-1+1
NBB=NBB
IF (N,LT,NB) NBB=N
DO 64 J=1,NBB
LJ=N-J+1
AJA1=V.X(LI,LJ)
KAUX1=KAX(LI,LJ)
CALL FLTGR (AJA2,KAUX2,BH(I,J),KB(I,J),A.X1,KAUX1)
CALL FLTGA (AJAY,KAUY,A.IA2,KAUX2,F.)
64 CONTINUE

C
DO 966 I=1,MA
JA=1
IF (I,E+1) JA=C
NBB=NA
IF (N,LT,NA) NBB=N
LI=MA-1+1
IF (NBB,LT,JA) GO TO 906
DO 66 J=JA,NB
LJ=N-J+1
AJX1=VNYNT(LI,LJ)
KAUX1=KAYNT(LI,LJ)
CALL FLTGR (AJA2,KAUX2,AA(I,J),KA(I,J),A.IX1,KAUX1)
CALL FLTGA (AJAY,KAUY,A.IA2,KAUX2,F.)
66 CONTINUE
966 CONTINUE

C
IF (AUXY) 400,401,400
400 Y(MA,N)=AJAY+C.DU*KAU(XY
GO TO 402
401 Y(MA,N)=0.00
402 VNYNT(-A,I)=MJAY
KAYNT(-A,N)=KAUY
AJA1=S10RC(N)-Y(-A,N)

```

```
ERMS=EW45+AUX1*AUX1
IF(DAHS(AUX1).GE.ERMAX) ERMAX=AUX1
62 CONTINUE
942 CONTINUE
ERMSH0=ERMS/HY
ERMS=EW45/(MM*NN)
RETURN
END
```

## SUBROUTINE SHFTUR

```

C
C PURPOSE : AN AUXILIARY SUBROUTINE FOR SUBROUTINE SDFZDR.
C
C
C COMMON/JFCUR1/INDQCL,INDWIL
COMMON/JFCUR2/MA,NB,MB,NB,MM,NN,INSTORE
COMMON/SHFT1/STORE(128)
COMMON/JFCUR4/VNYNT(4,128),VNX(4,128),KAX(4,128)
LOGICAL INDQCL,INDWIL,KAUX1L
DOUBLE PRECISION STORE,AUX1,AUX2,FREE,VNX,VNYNT

C
DO 1 I=2,MB
DO 1 J=1,NN
VNX(I-1,J)=VNX(I,J)
1 KAX(I-1,J)=KAX(I,J)
1 KAUX1L=INDWIL
DO 2 J=1,NN
AJA1=STORE(J)
CALL FLTGH(AJA1,AUAZ,KAUX1L,FEE)
VNX(MB,J)=AUAZ
2 KAX(MB,J)=KAUX2
2 KAUX1L=INDWIL
DO 4 I=2,MA
DO 4 J=1,NN
VNYNT(I-1,J)=VNYNT(I,J)
4 KAYNT(I-1,J)=KAYNT(I,J)
CALL IJP(2MB,2,STORE,INSTURE)
RETURN
END

```

SUBROUTINE FLTUA (VN1,KA1,VN2,KA2,INUPL)

```

C
C PUPPOSE:
C   TO SIMULATE DECIMALLY THE BINARY ADDITION (OR SUBTRACTION)
C   OF TWO FLTGR=PT. NUMBERS (VN1*2.D0D0**((KA1))) AND (VN2*2.D0D0**((KA2))).
C
C
C   SUBROUTINE NEEDS:
C     QNTZD.
C
C   INPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS):
C     VN1,VN2,KA1,KA2,INUPL,EU,EOH,EOI,DL2,IS
C
C   OUTPUT ARGUMENTS:
C     VN1,KA1
C
C   DESCRIPTIONS OF INPUT AND OUTPUT ARGUMENTS:
C
C   VN1,KA1: AS INPUTS, PLEASE SEE (PUPPOSE).
C             AS OUTPUTS, TO STORE THE RESULTS OF THE ADDITION
C             OR SUBTRACTION.
C
C   VN2,KA2: PLEASE SEE (PUPPOSE).
C
C   INUPL,T,: INDICATING (VN1*2.D0D0**((KA1)) + (VN2*2.D0D0**((KA2))).
C             F.: INDICATING QUANTIZN. AND OVERFLOW LIMITN. DESIRED IN THE OPERATN.
C
C   INUQRL,T,: QUANTIZN. AND OVERFLOW LIMITN. DESIRED IN THE OPERATN.
C   EU,EOH,EUI,EUVER1,EOVER2,DL2,IS: PLEASE SEE SUBROUTINE FLTGR.
C
C   COMMON/QNTZD1/EU,EUM,EUI,EUVER1,EOVER2
C   COMMON/FLTGR1/DL2,IS
C   COMMON/FLTGM1/INUQRL
C   LOGICAL INUPL,INUQRL
C   DOUBLE PRECISION VN1,VN2,DL2,E0,EOH,SN,V1,EDI,EOVE,1+EOVER2
C
C
C   IF(VN2.EQ.0.00) RETURN
C   IF(VN1.EU.0.00) GO TO 10
C
C   N=KA1-KA2
C   NV=LAHS(1)
C   SN=2.D0**(-NV)
C   IF(N) 1,2,3
1  VN1=VN1*SN
   IF(INUQRL) CALL QNTZD (VN1,VN1)
   KA1=KA2
   GO TO 2
3  VN2=VN2*SN
   IF(INUQRL) CALL QNTZD (VN2,VN2)
2  IF(INUPL) VN1=VN1+VN2
   IF(.NOT.INUPL) VN1=VN1-VN2
   SN=DARS(VN1)
   IF(SN.EQ.1) GO TO 200
   IF(VN1.LT.1.D0.AND.VN1.GE.(-1.D0)) GO TO 41
   GO TO 400
200 IF(SN.LT.1.D0) GO TO 41
400 VN1=VN1*0.5D0
   IF(INUQRL) CALL QNTZD (VN1,VN1)
   KA1=KA1+1
   RETURN

```

```
41 IF(SN.GE.0.5UU.OH,SN.EQ.1.0D) RETURN
    CALL FLTGR(VIN1,VIN2,KA1,F1,F2,SN)
    KA1=KA1+KA2
    VV1=VN
    RETURN
100 VN1=VN2
    KA1=KA2
    IF(.NOT.INPUTL) VV1=-VV1
    RETURN
END
```

SUBROUTINE FLTGM (VN1,KAI,VN2,KA2,VN3,KA3)

```

C
C PURPOSE:
C   TO SIMULATE THE MULTIPLICATION OF TWO FLOATING-POINT
C   NUMBERS (VN2*2.0D**KA1) AND (VN3*2.0D**KA3). THE
C   RESULTS ARE STORED AS (VN1*2.0D**KA1).
C
C SUBROUTINE NEEDS:
C   QMTZD.
C
C INPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS):
C   VN2,KA2,VN3,KA3,EU,EOH,EOT,UL2,IS
C
C OUTPUT ARGUMENTS:
C   VN1,KAI
C
C DESCRIPTIONS OF INPUT AND OUTPUT PARAMETERS:
C
C VN1,VN2,VN3,KAI,KA2,KA3: PLEASE SEE (PURPOSE).
C EU,EOH,EUI,EUVER1,EUVER2,UL2,IS: PLEASE SEE SUBROUTINE FLTGR.
C INQURL=.T.: QUANTIZATION OF MULTIPLICATION IN THE OPERATION DESIRED.
C
C COMMON/QMTZD/EU,EUH,EUI,EUVER1,EUVER2
C COMMON/FLTGR/UL2,IS
C COMMON/FLTGM1/INQRL
C DOUBLE PRECISION VN1,VN2,VN3,EU,EOH,EUI,UL2,VN,EUVER1,EUVER2
C LOGICAL INQRL

C
C
C IF(VN3.EQ.0.0D+0.0D) GO TO 100
C KAI=KA2+KA3
C VN1=VN2*VN3
C IF(INQRL) CALL QMTZD (V11,VN1)
C IF(DABS(VN1)=0.5D0) 10.129,129
C 10 VN1=VN1*2.0D
C KAI=KAI-1
C GO TO 129
C 100 KAI=0
C VN1=0.0D
C 129 RETURN
C END

```

SUBROUTINE FLTGK (VN,VN,KA,INDQL,INDQVL,V1)

1634 IF (INDLVL) .NE. 2.0 RETURN  
END

SUBROUTINE QNTZD (V,VNN)

```

C
C PURPOSE:
C   TO QUANTIZE A NUMBER (INCLUDING OVERFLOW LIMITATION).
C
C INPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENT):
C   V,E0,E0M,E0I,E0VER1,E0VER2
C
C OUTPUT ARGUMENTS:
C   VNN
C
C DESCRIPTIONS OF INPUT AND OUTPUT ARGUMENTS:
C
C E0: QUANTIZATION LEVEL OR STEP SIZE.
C E0M: HALF OF E0.
C E0I: 1.00/E0.
C V: THE NUMBER TO BE QUANTIZED AND LIMITED.
C VNN: THE OUTPUT NUMBER.
C E0VER1,E0VER2: THE LOWER LIMIT AND THE UPPER LIMIT FOR VNN.
C
C DOUBLE PRECISION V,VNN,E0,E0M,D ,VNN,E0I,E0VER1,E0VER2
C COMMON/QNTZD/E0,E0M,E0I,E0VER1,E0VER2
C
C
V1=V
K=V*E0I
V4=E0*FLOAT(R)
D=V-VN
VN=VN
IF(V1) 1,2,2
1 IF (D.LE.(-E0M)) VN=V4-E0
   IF(VNN.LT.E0VER2) VN=E0VER2
   GO TO 900
2 IF (D.GE.E0M) VN=V4+E0
   IF(VNN.GT.E0VER1) VN=E0VER1
900 RETURN
END

```

## PROGRAM OFI11 (INPUT, OUTPUT)

C  
C  
C

## PURPOSE :

TO ANALYZE THE ERROR PROPERTIES FOR ONE-DIMENSIONAL DIGITAL FILTERS EXPLOITING FLOATING-POINT ARITHMETIC BY USING SUBROUTINES DFZIO AND DFZOH TO ESTIMATE MEAN SQUARE ERRORS AND NORM ERROR BOUNDS AND TO COMPARE THEM WITH THE ACTUAL ERRORS OBTAINED THROUGH SIMULATIONS.

C  
C  
C

## SUBROUTINES NEEDED :

DFZIO, DFZOH, NOISE, FLTGA, FLTGM, FLTGR, QNTZD, FREQZ1.

C  
C  
C

## INPUT ARGUMENTS BY (FORTRAN IV) READ STATEMENTS :

NA, NB, NN, IPRTN, IS, NT1, NT2, NTINCR, INDX, I, WJ, STD, BMFY,  
START, STD2, START2, A, B.

C  
C

## DESCRIPTIONS OF INPUT ARGUMENTS :

C  
C  
C

NA, NB, NN, A, B : PLEASE SEE SUBROUTINE DFZIO.  
IPRTN=-1 : THE FORTRAN VARIABLE NPRINT (PLEASE SEE SUBROUTINE DFZIO) WILL BE GIVEN THE VALUE (-1).

C  
C  
C

IPRTN=0 : NPRINT=NN/55+1.

IPRTN = 0 : NPRINT=NN/IPRTN+1.  
IS=1 : SIGN AND MAGNITUDE REPRESENTATION FOR MANTISSA OF A FLOATING-POINT NUMBER IN SIMULATING OPERATIONS OF THE DIGITAL FILTERS.  
NT1, NT2, NTINCR : THE SIMULATIONS AND ESTIMATIONS WILL BE DONE FOR  
T (NUMBER OF BINARY BITS) = NT1, NT1+NTINCR, NT1+2  
...+NTINCR,...,(AROUND) NT2.

C  
C  
C

INDQ=-1 : ERROR ANALYSIS FOR INPUT QUANTIZATION ONLY (I).  
INDQ= 0 : ERROR ANALYSIS FOR COEFFICIENT QUANTIZN. ONLY (C).  
INDQ= 1 : ERROR ANALYSIS FOR ROUND OFF ERROR ONLY (R).  
INDQ= 2 : ERROR ANALYSIS FOR COEFFICIENT QUANTIZATIONS AND  
ROUNDOFF ERRORS (R AND C).  
INDQ= 3 : ERROR ANALYSIS FOR INPUT AND COEFFICIENT QUANTIZATIONS  
AND ROUNDOFF ERRORS (R, C AND I).

C  
C  
C

INDQ= 4 : CASES FOR INDQ=0, 1, AND 2.  
INDQ= 5 : CASES FOR INDQ=-1, 0, 1, 2, AND 3.

INDX, AMP, I, WJ, STD, START, STD2, START2 :

C  
C  
C

PARAMETERS FOR ASSIGNING THE INPUTS TO THE DIGITAL FILTER.  
(PLEASE SEE THE SECTION FOR INPUT SET-UP IN THIS PROGRAM).  
INDA=5 OR <5, ONLY ONE OF THE NINE KINDS OF INPUTS IS USED FOR  
ERROR ANALYSIS, IND=6 OR >6, NINE KINDS OF INPUTS ARE USED.

C  
C  
C

BMFY=0 : NO MODIFICATIONS FOR THE FILTER NUMERATOR COEFFICIENTS, B(I).

BMFY=1 : ALL B(I) ARE DIVIDED BY B(1)/1.2.

BMFY=2 : ALL B(I) ARE DIVIDED BY BMFY.

C  
C  
C

## COMMENTS :

1. THE MAXIMUM VALUE OF THE AMPLITUDE FREQUENCY RESPONSE IS OBTAINED BY SUBROUTINE FREQZ1. IT IS AN APPROXIMATED VALUE, AND THE ACCURACY DEPENDS ON THE PARAMETER SETUPS FOR AND THE WAY OF USING SUBROUTINE FREQZ1.
2. THE COMPUTATION TIME FOR THIS PROGRAM AT INDX=6, INDQ=5, NT1=8,  
NT2=29, AND NTINCR=7 IS APPROXIMATELY 200 SEC FOR A FIFTH ORDER FILTER WITH ALL THE COEFFICIENTS NOT EQUAL TO 0 OR 1. IF NO SIMULATIONS ARE INVOLVED, 12 SEC IS NEEDED UNDER THE SAME CONDITIONS.

C  
C  
C

```

COMMON/DF2I1/A(8),B(8),Y(256),X(256)
COMMON/DF2I2/NA,NB,NN,NPRINT
COMMON/DF2I8/YNT(256)
COMMON/FLTGM1/INDQRL/DF2DR1/INDQCL,INDQIL
COMMON/FLTGR1/DL2,IS
COMMON/JNTZD1/E0,EDH,EOVER1,EOVER2
COMMON/DFEUR4/VNYNT(256),VNX(256),KAYNT(256),KAX(256)
DIMENSION ERMST(S),ERMSTO(S),PLINE(130),ERMSTB(S),ERMSTBO(S)
DOUBLE PRECISION A,B,Y,X,EDH,DL2,MY,VNYNT,VNX,EDI,
*HR,MI,MX,EOVER1,EOVER2,YNT
LOGICAL INDQRL,INDQCL,INDQIL,INDIL
DATA P/1H*/
```

C  
C

```

1400 FORMAT(1H,/)
1432 FORMAT(1X,*THE ACTUAL OUTPUTS AT FINITE BITS : /*1X*(11D11+3))
1486 FORMAT(1X,*THE MAXIMUM AMPLITUDE FREQUENCY RESPONSE FOR THE WHOLE
*FILTER I *,E13.5)
1485 FORMAT(1X,*THE MAXIMUM AMPLITUDE FREQUENCY RESPONSE FOR THE DENOMI
*NATOR FILTER I *,E13.5)
1641 FORMAT(1X//1A,*ERROR BONUS I *//1X,*R I *,2E13.5/1X,*C I *,2E13.
*5/1X,*I I *,2E13.5/1X,*R AND C I *,2E13.5/1X,*R C AND I I *,2E13.5
*///)
1520 FORMAT(1X/1X,*THE INDICATOR FOR TYPE(S) OF INPUT(S) I *,I4//1X,*NT
*HEH INPUT PARAMETER VALUES ARE I *, YI4,3F7.2 /4X,*RESPECTIVELY FOR
* NA, NH, IERRDN, IS, VT1, NT2, NTINCR, IND3, IPHNT, HMFY, STD2, ST
*ART2,*///)
1167 FORMAT(1X,*THE SQRE SUM OF THE IDEAL OUTPUT SIGNAL IS*,D17.5/1X,
**THE INDICATORS FOR ROUNDOFF ERROR OPERATIONS, COEFFICIENT AND IN
*PUT QUANTIZATIONS ARE INDURL, INDQCL, AND INDQIL, RESPECTIVELY*/
*/*1X,*THEIR VALUES FOLLOW THE NUMERICAL VALUES OF THE ACTUAL ERRORS
*.*//)
1003 FORMAT(1X,9Fd.4)
1000 FORMAT(1X,1914)
1001 FORMAT(1X,5D13.6)
1601 FORMAT(1X//1X,*ESTIMATED ERRORS AND ACTUAL ERRORS AT*,I3,* BITS I
*///1X,*ESTIMATED ERRORS I *//1X,*R I *,2E13.5/1X,*C I *,2E13.5)
1603 FORMAT(1X,I I *,2E13.5/1X,*R AND C I *,2E13.5/1X,*R C AND I I *,
*2E13.5//)
1405 FORMAT(1X,*R C AND I I *,3E13.5,4X,*INDICATOR VALUES I *,3L3,
*6X,*EST. ER./ACT. I *,3X,F5.2)
1406 FORMAT(1X,*R AND C I *,3E13.5,6X,*INDICATOR VALUES I *,3L3,
*6X,*EST. ER./ACT. I *,3X,F5.2)
1403 FORMAT(1X,*R I *,3E13.5,13X,*INDICATOR VALUES I *,3L3,
*6X,*EST. ER./ACT. I *,3X,F5.2)
1402 FORMAT(1X,I I *,3E13.5,13X,*INDICATOR VALUES I *,3L3,
*6X,*EST. ER./ACT. I *,3X,F5.2)
1401 FORMAT(1X,*C I *,3E13.5,13X,*INDICATOR VALUES I *,3L3,
*6X,*EST. ER./ACT. I *,3X,F5.2)
1010 FORMAT(1H1,*AMPLITUDE (MAX VALUE) I *,E13.5/1X,*FREQUENCIES FOR S1
*NJSOIJAL INPUTS I *,E13.5,* (WI) I *,E13.5,* (WJ) /*1X,*STARTING
*VALUE AND STANDARD DEVIATION FOR NOISE INPUT GENERATN. I *,2E13.5)
1011 FORMAT(1X,*NUMBER OF INPUT OR OUTPUT POINTS I * *
*I6//1X,*THE FILTERING COEFFICIENTS ARE I */
1510 FORMAT(1X,13U11.12)
1501 FORMAT(1X,*INPUTS ARE AMP COS(10 WJ WI J).*)
1502 FORMAT(1X,*INPUTS ARE AMP C*S(WJ/(10 #I) J).*)
1503 FORMAT(1X,*INPUTS ARE AMP COS(WJ J).*)
1504 FORMAT(1X,*INPUTS ARE AMP NOISE.*)
```

```

1505 FORMAT(1x,*INPUTS ARE A*P NOISE COS(WJ J).*)
1506 FORMAT(1x,*INPUTS ARE A*P COS(WJ J + NOISE).*)
1507 FORMAT(1x,*INPUTS ARE AMP COS(NOISE J).*)
1508 FORMAT(1x,*INPUTS ARE AMP (X(J) COS(#J J)+YNT(J) COS(WJ J)).*)
1509 FORMAT(1x,*INPUTS ARE A*P (X(J) COS(#J J)+YNT(J) COS(WJ J)).*)
1012 FORMAT(1x,5D14.6)
1712 FORMAT(1x,///)

C
READ 1000,NA,NB,NN,IERORR,IS,NT1,NT2,NT1+CR,INDQ,INDX,IPRNT
READ 1003,AMP,WI,WJ,STD,HMFY,START,STD2,START2
READ 1001,(A(J),J=1,NA)
READ 1001,(H(J),J=1,NB)

C
DO 49 I=1,130
49 PLINE(I)=P
IF(IPRNT) 530,531,532
530 NPHINT=-1
GO TO 533
531 IPRNT=65
532 NPHINT=NN/IPRNT+1
533 IF(START.EQ.0.) START=0.5
DL2=1.00/DLOG(2.00)
IF(NT2.EQ.0.) NT2=NT1
IF(NT1.NE.0.) NTINCR=4
IF(WI.EQ.0.) *I=1.
IF(WI.EQ.1.) WJ=1.
IF(STD.EQ.0.) STD=0.1
IF(AMP.EQ.0.) AMP=1.
IF(HMFY) 264,265,266
264 HMFY=B(1)/1.2
266 DO 53 J=1,NB
 53 H(J)=H(J)/HMFY
 533 CONTINUE

C
PRINT 1011,AMP,WI,WJ,STD,START
PRINT 1011,NN
PRINT 1012,(A(J),J=1,NA)
PRINT 1012,(H(J),J=1,NB)
PRINT 1520,INDX,NA,NB,IERORR,IS,NT1,NT2+NT1+CR,INDU,IPRNT,HMFY,
*STD2,START2

C
C      CALCULATING THE MAXIMUM VALUE OF THE DENOMINATOR FILTER
C
C      PI=3.141592653589
MPT=180
WJST=0.
WJL=2.*PI
IJ=1
C
CALL FREQZ1 (IU,MPT,WJST,WJL,WJMAX,HMAX)
PRINT 1485,HMAX
C
ID=0
WJL=2.*PI
WJST=0.
CALL FREQZ1 (IU,MPT,WJST,WJL,WJMAX,GMAX)
PRINT 1485,GMAX
HMAX=HMAX*HMAX
GMAX=GMAX*GMAX
C
C      SET UP INPUTS TO THE ONE-DIMENSIONAL DIGITAL FILTER.

```

```

C
IESTRPE=-1
IDINDEX=INDEX
NINDEX=n
IF(IDI+DX<NINDEX) GO TO 514
INDEX=-3
514 PRINT 1400
PRINT 1510,(PLINE(I),I=1,150),INDEX
IF(INDEX) <20,221,221
220 IF(INDEX+2) 371,372,373
373 DO 16 J=1,NN
16 X(J)=AMP*COS(*J*J)
INUPRT=3
GO TO C
372 WI=WJ*10.*#I
INUPRT=1
375 DO 71 J=1,NN
71 X(J)=AMP*COS(*I*J)
GO TO C
371 IF(IDI+DX,GE,NINDEX) WI=WI/(100.*WI**2)
IF(IDI+DX,LT,NINDEX) WI=WJ/(10.*WI)
INUPRT=2
GO TO 375
221 CALL NOISE(NN,STD,START)
IF(INDEX-1) 256,256,257
256 DO 231 J=1,NN
231 X(J)=AMP*A(J)
INUPRT=4
IF(INDEX.EQ.0) GO TO 2
DO 258 J=1,NN
258 X(J)=X(J)+COS(*J*J)
INUPRT=3
GO TO C
257 IF(INDEX-3) 257,250,256
259 DO 263 J=1,NN
263 X(J)=AMP*COS(WJ*J*X(J))
INUPRT=6
GO TO 2
260 DO 5264 J=1,NN
5264 X(J)=AMP*COS(X(J)*J)
INUPRT=7
GO TO C
266 IF(INDEX=5) 293,293,2
293 DO 79 J=1,NN
79 YNT(J)=X(J)
STD=STD*2
IF(STD.LE.0.) STD=STD*0.5123
START=START*2
IF(START.LE.0.) START=START*0.793
INUPRT=8
CALL NOISE (NN*STD*START)
IF(INDEX.EQ.5) GO TO 476
WK=WJ
477 DO 73 J=1,NN
73 X(J)=AMP*(X(J)*COS(WK*J)+YNT(J)*COS(*J*J))
GO TO 2
476 WK=WJ
IF(WK.EQ.WJ) WK=1.*#WJ
INUPRT=9
GO TO 477
2 CONTINUE
GO TO (501,502,503,504,505,506,507,508,5,91),INUPRT

```

```

501 PRINT 1511
GO TO 515
502 PRINT 1512
GO TO 515
503 PRINT 1513
GO TO 515
504 PRINT 1514
GO TO 515
505 PRINT 1515
GO TO 515
506 PRINT 1516
GO TO 515
507 PRINT 1517
GO TO 515
508 PRINT 1518
GO TO 515
509 PRINT 1519

C 515 PRINT 1510,(PLINE(I),I=1,130),INDX
C
INDQAX=INDW
DO 10 I=N1,NTC,NTINCR
EO=2.DU**(-I)
EDI=2.DU**I
EOH=EO*0.5D0
EOVER1=1.DU-EO
EOVER2=-EOVER1
IF (IS.E,1) EOVER1=-1
IF (I.G1.NT1) IESTRP=1
CALL DF2I (IESTRP,EHMST,EHMST0,HY,EO*EO,HP,-I,MX,UM,X,HMAX,
*ERMSTB,ERMSTB0)
PRINT 1611,I*((EHMST(I))+EHMST0(I)),II=1,2)
PRINT 1603,((EHMST(I)),EHMST0(I)),II=3,5)
IF (I.EV.NT1) PINT 1167,HY
PRINT 1641,((ERMSTB(I)),ERMSTB0(I)),II=1,5)
INVIL=.F.
IF (IND0=4) 111,112,112
111 INDQRL=.F.
INDQCL=.F.
INDQIL=.F.
IF (INDQAX) 140,141,142
142 INDQRL=.T.
IF (INDQAX=2) 171,172,173
171 ASSIGN 403 TU ISWITCH
GO TO 144
172 INDQCL=.T.
ASSIGN 404 TU ISWITCH
GO TO 144
173 INDQCL=.T.
INDQIL=.T.
ASSIGN 405 TU ISWITCH
GO TO 144
141 INDQCL=.T.
ASSIGN 401 TU ISWITCH
GO TO 144
140 INDQIL=.T.
ASSIGN 402 TU ISWITCH
144 CALL DF2DR (ERMAX,ERMS,ERMSR0,HY)
INDIL=.T.
GO TO ISWITCH,(4,1,402,403,404,405)
401 RT1=ERMSTU(2)/ERMSR0
PRINT 1471,ERMS,ERMSR0,ERMAX,INDQRL,INDQCL,INDQIL,.T1

```

```

      GO TO 165
402 RT1=ERMSRO
      PRINT 1402,ERMS,ERMSRO,ERMAX,INDQRL,INDQAL,INDQIL,RT1
      GO TO 165
403 RT1=ERMSTU(1)/ERMSRO
      PRINT 1403,ERMS,ERMSRO,ERMAX,INDQRL,INDQAL,INDQIL,RT1
      GO TO 165
404 RT1=ERMSTU(4)/ERMSRO
      PRINT 1404,ERMS,ERMSRO,ERMAX,INDQRL,INDQAL,INDQIL,RT1
      GO TO 165
405 RT1=ERMSTU(5)/ERMSRO
      PRINT 1405,ERMS,ERMSRO,ERMAX,INDQRL,INDQAL,INDQIL,RT1
      GO TO 165
112 IF(INDU.EV.5) GO TO 167
      IAUX1=0
      ISTOP=2
      GO TO 168
167 IAUX1=-1
      ISTOP=3
168 IF(IAUX1.GE.1STOP) GU TO 10
      IF(INDIL) IAUX1=IAUX1+
      INDQAX=IAUX1
      GO TO 111
169 IF(INDQ.GT.3) GU TO 16H
      IF(NPRINT.LE.0) GO TO 543
      PRINT 1400
      PRINT 1432,(YNT(J):J=1,NN,NPRINT)
543 PRINT 1702
      10 CONTINUE
C
      IF(IDI>DX+LT+NINDEX) STOP
      IF(INDX.EG.(NINDEX-1)) STOP
      INDEX=I+DX+1
      IESTRP=0
      GO TO 514
      END

```

SUBROUTINE DFZIO (IESTRP, ERMST, ERMSTRU, HY, EOSURE, H4, HI, HX, GMX, HMX,  
#ERMSTH, ERMSTU)

C  
C  
PURPOSE :  
TO CALCULATE (1) THE MEAN SQUARED ERROR ESTIMATIONS AND (2) THE  
NORM ERROR BOUNDS FOR ALL SOURCES OF ERROR IN ONEDIMENSIONAL DIGITAL  
FILTERS EMPLOYING FLOATING-POINT ARITHMETIC.

C  
C  
SUBROUTINES NEEDED :  
FLTGR, WNTZU.

C  
C  
INPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
IESTRP, HY, EOSURE, H4, HI, HX, GMX, HMX, A, B, X, VA, NB, NN, NPRINT.

C  
C  
OUTPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
ERMST, ERMSTRU, ERMSTH, ERMSTU, HY, HH, HI, HX, Y.

C  
C  
DESCRIPTIONS OF INPUT AND OUTPUT ARGUMENTS :  
C

IESTRP=1 : NO CALCULATIONS FOR HH, H, AND HX.

IESTRP=0 : NO CALCULATIONS FOR HH AND H.

IESTRP=-1 : CALCULATIONS FOR HH, H, AND HX.

ERMST(I) : TO STORE THE ESTIMATED OUTPUT MEAN SQUARED ERROR.

HY : THE OUTPUT SQUARE SUM.

ERMSTRU(I) : ERMST(I)/HY.

EOSURE : EO\*EU, WHERE EO IS THE QUANTIZATION STEP SIZE.

HH : THE IMPULSE RESPONSE SQUARE SUM FOR THE DENOMINATOR FILTER.

HI : THE IMPULSE RESPONSE SQUARE SUM FOR THE NUMERATOR FILTER.

HX : THE INPUT SQUARE SUM.

GMX : THE SQUARED VALUE OF THE MAXIMUM AMPLITUDE FREQUENCY RESPONSE

FOR THE WHOLE FILTER.

HMX : THE SQUARED VALUE OF THE MAXIMUM AMPLITUDE FREQUENCY RESPONSE

FOR THE DENOMINATOR FILTER.

ERMSTH(I) : TO STORE THE ESTIMATED NORM ERROR BOUND.

ERMSTU(I) : ERMSTH(I)/HY.

ERMSTRU(I), VA, NB : STORING THE COEFFICIENTS OF THE DIGITAL FILTER.

A(I), B(I), VA, NB : THAT IS,  $(B(1)+B(2)*Z^{*-1}+\dots+B(NB)*Z^{*(-NB+1)})$

$+))/((A(1)+A(2)*Z^{*-1}+\dots+A(NA)*Z^{*(-NA+1)})$

NN : NUMBER OF POINTS OF THE FILTERING OPERATIONS.

NPRINT > 0 : PRINT OUTPUTS FOR ONE OUT OF EVERY (NPRINT) POINTS OF

THE INPUTS AND OUTPUTS OF THE FILTER.

OTHERWISE : NO PRINT OUTPUTS FOR THE INPUTS AND OUTPUTS.

X(I), I=1,...,NN : THE INPUTS OF THE DIGITAL FILTER.

Y(I), I=1,...,NN : THE OUTPUTS OF THE DIGITAL FILTER.

C  
C  
COMMON/DFZI1/A(8),B(8),Y(256),X(256)  
COMMON/DFZI2/VA,NB,NN,NPRINT  
COMMON/DFZI8/YNT(256)  
DIMENSION YMA(8),YMB(4),ALPHA(8),BETA(8),QEA(A)  
#,ERMST(5),ERMSTRU(5),QEBO(8),ERMSTH(5),ERMSTU(5)  
LOGICAL IAUX1,INDAL  
DOUBLE PRECISION A,B,Y,X,YMA,YMB,V,MY,HH,ALPHA,BETA,QEA,HD,HB,  
\*STORE,H,EOASURE,AUX1,AUX2,FRFE,HX,HBRN4,HR,YNT,HI,QEBO,HB,NN  
IF(IESTRP) 191,191,192  
191 00126 J=1,NN

```

120 Y(J)=0.00
    DO 81 J=1,NN
    81 YT(J)=A(J)
    DO 24 J=1,NA
    24 YM(J)=0.00
    00124 J=1,NB
    124 YM(B(J))=0.00
C
C      PREPARE TO FIND OUTPUT Y WITH REGULAR INPUT X.
C
    HX=0.00
    H=0.00
    INDT=2
    INDAL=.T.
    IND=1
    IAUX1L=.F.
C
    047 DO 62 I=1,NN
        Y(N)=0.00
        GO TO (544,700),INDT
C
    700 DO 964 J=1,NB
        LJ=N-J+1
        IF(LJ.LT.1) GO TO 964
        V=X(LJ)*B(J)
        Y(N)=Y(V)+V
        GO TO (64,674),INDT
    674 YM(B(J))=YM(B(J))+V*V
    64 CONTINUE
    964 CONTINUE
C
    GO TO 645
C
    644 IF(IAUX1L) GO TO 645
    IF(IND) 679,669,679
    679 Y(N)=1.00
    GO TO 659
    669 IF(N.GT.(NB+1)) GO TO 659
    X(N)=0.00
    IF(N.EQ.1) X(N)=1.00
    GO TO 700
    659 IAUX1L=.T.
C
    645 DO 66 J=2,NA
        LJ=N-J+1
        IF(LJ.LT.1) GO TO 66
        V=Y(LJ)*A(J)
        Y(N)=Y(V)-V
        GO TO (66,676),INDT
    676 YM(A(J))=YM(A(J))+V*V
    66 CONTINUE
C
    H=H+Y(N)*Y(N)
    IF(INDAL) HX=HA+X(N)*X(N)
    62 CONTINUE
C
C      IF(IND) 701,640,702
    701 HH=H
    IAUX1L=.F.
    IND=0
    INDT=1

```

```

H=0.00
PRINT 177,J,HN
IF(NPRINT) 801,B61,B62
851 PRINT 1235,Y(1),Y(NN)
GO TO 547
852 PRINT 1635,(Y(J)+J=1,NN,NPRINT)

C      GO BACK TO FIND THE IMPULSE RESPONSE FOR THE WHOLE FILTER.
C
C      GO TO 547
C
C      702 H=M
C
C      IF(IESTRP) 743,744,743
C
C      PREPARE TO GO BACK TO FIND THE IMPULSE RESPONSE FOR THE
C      DENOMINATOR FILTER.
C
C      743 IND=-1
C      INDGT=1
C      H=0.00
C      INDXL=.F.
C      INDULL=.F.
C      DO 29 J=1,NN
C      29 X(J)=Y(J)
C      NXSTRE=NH+1
C      DO 31 J=1,NXSTRE
C      31 QEA(J)=X(J)
C      GO TO 547

C      SET UP VARIOUS VALUES FOR ERROR ESTIMATIONS.
C
C      646 H=M
C***** THE FOLLOWING STATEMENTS SHOULD BE PROPERLY ADJUSTED WHEN ONE OR
C***** MORE OF THE FILTER COEFFICIENTS IS ZERO, OR ONE.
C***** 744 DO824 J=1,NB
C      IF(J,EQ.1) BETA(J)=(NB)
C      IF(J,NE.1) BETA(J)=(NB-J+1)
C
C      874 CONTINUE
C      DO 26 J=1,NA
C      IF(J,EQ.2) ALPHA(J)=NA
C      IF(J,NE.2) ALPHA(J)=(NA-J+2)
C      IF(J,EQ.1) ALPHA(J)=U.
C
C      26 CONTINUE
C***** 1F(IESTRP,GE,1) GO TO 799
C      DO 35 J=1,NXSTRE
C      35 X(J)=QEA(J)
C      799 DO224 J=1,NB
C      224 QEB0(J)=YMB(J)/3.00*BETA(J)
C      DO 226 J=1,NA
C      226 QEA(J)=YMA(J)/3.00*ALPHA(J)
C
C      192 HR=0.
C      DO 228 J=1,NA
C      228 HR=HR+QEA(J)
C      HBRNM=1.00
C      DO 230 J=1,NB
C      230 HBRNM=HBRNM+QEB0(J)

```

```

C
HJ=0.
HNMM=0.0
DO 771 J=1,NN
AUX1=B(J)
CALL FLTGR(AUX1,FREE,KAU1,T0,T0,AUX2)
AJX1=((AU1-AJX2)/AU1)**2
771 HBNM=HBNM+YMD(J)*AUX1
DO 772 J=1,NN
AUX1=A(J)
CALL FLTGR(AUX1,FREE,KAU1,T0,T0,AUX2)
AJX1=((AU1-AJX2)/AU1)**2
772 HD=HD+YMA(J)*AUX1
IF(IESTRM) 548,547,539
548 PRINT 1774,H
IF(NPR1NT) 865,865,866
865 PRINT 123U,Y(1),Y(NN)
GO TO 567
866 PRINT 1646,(Y(J),J=1,NN,NPRINT)
867 PRINT 1400
PRINT 1400
DO 39 J=1,NN
39 Y(J)=X(J)
DO 86 J=1,NN
86 X(J)=YNT(J)
547 IF(NPR1NT) 549,539,869
869 PRINT 1547,(Y(J),J=1,NN,NPRINT)
PRINT 1400
PRINT 1638,(A(J),J=1,NN,NPRINT)
539 CONTINUE

C
C   ROUNDOFF ERRORS ESTIMATION
C
ERMST(1)=(HR+HBRNM)*HH*EUSURE
ERMSTRU(1)=ERMST(1)/HY
ERMST(1)=ERMST(1)/NN

C
C   ESTIMATION OF COEFFICIENT QUANTIZATION ERRORS
C
ERMST(2)=(HD+HBNM)*HH
ERMSTRU(2)=ERMST(2)/HY
ERMST(2)=ERMST(2)/NN

C
C   ESTIMATION OF INPUT QUANTIZATION ERRORS
C
ERMST(3)=MX*H1*EUSURE/3.0D0
ERMSTRU(3)=ERMST(3)/HY
ERMST(3)=ERMST(3)/NN

C
C   ESTIMATION OF ERMST(1)+ERMST(2)
C
ERMST(4)=ERMST(1)+ERMST(2)
ERMSTRU(4)=ERMSTRU(1)+ERMSTRU(2)
ERMST(5)=ERMST(4)+ERMST(3)
ERMSTRU(5)=ERMSTRU(4)+ERMSTRU(3)

C
C   ESTIMATION OF NORM ERROR BOUNDS
C
ERMSTB(1)=(HH+HBRNM)*HMX*EUSURE
ERMSTB(2)=(HU+HBNM)*HMX
ERMSTB(3)=HMX*GMX*EUSURE/2.0D0
ERMSTBU(1)=ERMSTB(1)/HY
ERMSTBU(2)=ERMSTB(2)/HY

```

```
      ERMSTH(3)=ERMSTH(3)/HY
      ERMSTH(1)=ERMSTH(1)/NN
      ERMSTH(2)=ERMSTH(2)/NN
      ERMSTH(3)=ERMSTH(3)/NN
      ERMSTH(4)=ERMSTH(1)+ERMSTH(2)
      ERMSTH(5)=ERMSTH(4)+ERMSTH(3)
      ERMSTH(6)=ERMSTH(1)+ERMSTH(2)
      ERMSTH(7)=ERMSTH(4)+ERMSTH(3)

C
1638 FORMAT(1X,1I011.3)
1773 FORMAT(1X//1A,*THE IMPULSE RESPONSE SQRE SUMS OF THE*,
** DENOMINATOR FILTER IS *,D17.10)
1230 FORMAT(1X,*THE FIRST AND THE LAST VALUES OF THE RESPONSES ARE *,
*2D14.5,* RESPECTIVELY.*)
1774 FORMAT(1X//1A,*THE IMPULSE RESPONSE SQRE SUM OF THE*,
** WHOLE FILTER IS *,12X,D17.10)
1400 FORMAT(1H '/')
1547 FORMAT(1X,*THE REGULAR OUTPUTS AND INPUTS IS *//(1X,1I011.3))

C
      RETURN
      END
```

## SUBROUTINE DFZD0 (ERMAX, ERMS, ERMSR0, HY)

C  
C PURPOSE :  
C TO SIMULATE THE OPERATIONS OF ONE-DIMENSIONAL DIGITAL  
C FILTER EMPLOYING FLOATING POINT ARITHMETIC.  
C

C SUBROUTINES NEEDED :  
C FLTGA,FLTGR,FLTGM,INTZD.

C INPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
C HY,A,B,Y,X,NA,NB,NN ; PLEASE SEE SUBROUTINE DFZ10.  
C EO,EOM,EU1,EUVER1,EOVER2,DL2,IS ; PLEASE SEE SUBROUTINE FLTGR.

C INUQRL=T. ; SIMULATIONS INCLUDING ROUNDOFFS.  
C INUQCL=T. ; SIMULATIONS INCLUDING COEFFICIENT QUANTIZATIONS.  
C INUQIL=T. ; SIMULATIONS INCLUDING INPUT QUANTIZATIONS.

C ERMAX ; THE MAXIMUM ACTUAL ERROR.  
C ERMS ; THE ACTUAL MEAN SQUARED ERROR.  
C ERMSR0 ; ERMS/HY.  
C Y(I),I=1,...,NN ; THE ACTUAL OUTPUTS OF THE DIGITAL FILTER.  
C C C

COMMON//TZD1/EU,EOM,EOI,EUVER1,EOVER2  
COMMON//FLTGR1/DL2,IS  
COMMON//DFZ11//A(B),B(B),Y(256),X(256)  
COMMON//DFZ18/YNT(256)  
COMMON//DFZ12/NA+NBN,NN,NPRINT  
COMMON//FLTGM1/INUQRL/DFZDR1/INUQCL/INUJIL  
COMMON//DFZDR1/VNYNT(256),VNX(256),KAYVT(255),KAX(256)  
DIMENSION AA(B),BB(B),KA(B),KB(B)  
LOGICAL INUQRL,INUQCL,INUQIL,KAUXIL  
DOUBLE PRECISION A,B,Y,X,YNT,AA,BB,EU,EOM,DL2,HY,FREE,VNYNT,VNX,  
\*STORE,AUX1,AUX2,AUY1,EOI,EUVER1,EOVER2

C  
C ERMS=0.  
C ERMAX=0.  
C  
KAUXIL=INUQCL  
DO 32 J=1,NA  
AUX1=A(J)  
32 CALL FLTGR (AUX1,AA(J),KA(J),KAUX1L,,F,,FREE)  
DO 30 J=1,NB  
AUX1=B(J)  
30 CALL FLTGR (AUX1,BB(J),KB(J),KAUX1L,,F,,FREE)

C  
C  
UD 24 J=1,NN  
VNYNT(J)=0.0  
24 KAYNT(J)=0  
KAUX1L=INUJIL

```

DO 24 I=1,NN
AUX1=X(1)
CALL FLTGH(AUX1,AUX2,KAUX2,KAUX1L,,FR=F)
VNX(I)=AUX2
20 KAA(I)=KAUX2

C
DO 62 N=1,NN
AJAY=U,U
KAUXY=U

C
NBB=NH
IF(NLT,NB) NBB=N
DO 64 J=1,NBB
LJ=N-J+1
AUX1=VN(X(LJ))
KAUX1=KAA(LJ)
CALL FLTGM (AJX2,KAUX2,BH(J),KB(J)+AUX1,KAJX1)
CALL FLTGA (AJAY,KAUXY,AUX2+KAUX2+1)
54 CONTINUE

C
JA=2
NBB=NA
IF(N,LT,NA)NBB=N
IF(NBB,LT,JA) GO TO 70966
DO 66 J=JA,NBB
LJ=N-J+1
AUX1=VN(YNT(LJ))
KAUX1=KAYNT(LJ)
CALL FLTGM (AJX2,KAUX2,AA(J),KA(J)+AUX1,KAJX1)
CALL FLTGA (AJAY,KAUXY,AUX2+KAUX2+1)
56 CONTINUE
560 CONTINUE

C
IF(AUXY) 400,401,400
400 YNT(N)=AJAY*Z,UU**KAUXY
GO TO 402
401 YNT(N)=U,U
402 VN(YNT(N))=AUXY
KAYNT(N)=KAUY
AJX1=Y(N)-YNT(N)
ERMS=ERMS+AUX1*AUX1
IF(DABS(AUX1).GE.ERMAX) ERMAX=AUX1
62 CONTINUE
620 CONTINUE
620 ERMSU=ERMS/HY
ERMS=ERMS/NN
RETURN
ENU

```

SUBROUTINE NOISE(N,STD,START)

PURPOSE :  
TO GENERATE A NOISE SIGNAL WITH SUBROUTINE RANF.

INPUT ARGUMENTS :  
N,STD,START.

OUTPUT ARGUMENT (IN COMMON STATEMENT) :  
X.

DESCRIPTIONS OF INPUT AND OUTPUT ARGUMENTS :

N : NUMBER OF POINTS DESIRED.

STD : STANDARD DEVIATION.

START : STARTING VALUE FOR SIGNAL GENERATION.

X(I),I=1,...,N : GENERATED SIGNAL.

COMMON/DF2I1/A(8),B(8),Y(256),X(256)  
DOUBLE PRECISION A,B,X,Y

```

C PI=3.1415927
C IF(START) 1,2,3
1  DUMBERANF(START)
2  DO31=1,N
3  X(1)=(-2.*ALOG(RANF(0.)))**0.5
   X(I)=STD*X(I)*COS(2.*PI*RANF(0.))
   RETURN
END

```

SUBROUTINE FREUZ1 (IU,MPT,WJST,WJL,WJMAX,AMAX)

PURPOSE :  
TO CALCULATE THE FREQUENCY RESPONSE (AMPLITUDE) OF A  
ONE-DIMENSIONAL DIGITAL FILTER.

NOTE :  
THIS SUBROUTINE CAN BE MODIFIED TO DO THE SAME JOB FOR  
TWO-DIMENSIONAL DIGITAL FILTER.

SUBPROGRAM NEEVEU:  
CPV.

INPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
IU,MPT,WJST,WJL,A,B,NA,NB.  
OUTPUT ARGUMENTS (INCLUDING THOSE IN COMMON STATEMENTS) :  
WJST,WJL,WJMAX,AMAX,Y.

DESCRIPTIONS OF INPUT AND OUTPUT ARGUMENTS :  
ID=1 : CALCULATIONS OF FREQUENCY RESPONSE ARE FOR THE WHOLE FILTER.  
ID=0 : CALCULATIONS ARE FOR THE DENOMINATOR FILTER.  
WJL (AS INPUT) : LENGTH OF FREQUENCY RANGE.  
MPT, WJST (AS INPUT) : THE CALCULATIONS WILL BE ON THE FOLLOWING  
FREQUENCY POINTS. WJST,WJST+WJINC,WJST+2\*WJINC,...,  
WJST+(MPT-1)\*WJINC, WHERE WJINC=WJL/(MPT-1).  
A,B,NA,NB : FILTER COEFFICIENTS. (PLEASE SEE SUBROUTINE DF210).  
AMAX,WJMAX : THE MAXIMUM VALUE OF THE AMPLITUDE FREQUENCY RESPONSE  
IS AMAX, IT OCCURS AT THE FREQUENCY POINT WJMAX.  
Y(I), I=1,...,MPT : THE AMPLITUDE FREQUENCY RESPONSES.  
WJST (AS OUTPUT) : WJMAX=WJINC.  
WJL (AS OUTPUT) : WJINC\*2.

COMPLEX CPV,ZWJ,HZ(6),AZ(6),BZV,AZV  
COMMON/DF211/A(8),B(8),Y(256),X(256)  
COMMON/DF212/NA,NB,NN,NPHINT  
DOUBLE PRECISION A,B,Y,X  
LOGICAL ID,NBL

INITIAL SET UP:

```

      WJINC=WJL/(MPT-1)
      AMAX=0.
      IF(ID) 143,143,142
143 DO 142 J=1,NB
      AUX1=B(J)
142 BZ(J)=CMPLX(AUX1,0.)
      IDNML=.T.
      GO TO 144
144 DO 141 J=1,NA
      AUX1=A(J)
141 AZ(J)=CMPLX(AUX1,0.)
      ERANG=10.**(-B)

```

```

C      STARTING TO FIND THE FREQUENCY RESPONSE.
C
DO 1 M=1,MPT
WJ=WJST+WJICH*(M-1)
ZWJ=CMPLX(COS(WJ),SIN(WJ))
C
IF(IDN=IL) BZV=CPV(ZWJ,BZ,NB,J,NB)
AZV=CPV(ZWJ,AZ,NA,0,NA)
C
AHG=CAMS(AZV)
IF(AMG-ERANG) 120,120,123
120 AMG=10.**0
GO TO 125
123 AMG=CAMS(BZV)/AMG
125 Y(M)=A1G
IF(AMAX.GE.AMG) GO TO 1
AMAX=A1G
WJMAX=+J
1 CONTINUE
C
WJST=WJ-WJICH
WJL=WJICH*2.
RETURN
END

```

```
FUNCTION CPV (Z,AZ,NORDR1,NSTART,NTOTAL)

C
C      PURPOSE :          AN AUXILIARY PROGRAM FOR SUBROUTINE F/EZ1.
C
C
C      COMPLEX CPV,Z,AZ(NTOTAL)
C
C      CPV=CMPLX(0.,0.)
DO 24 I=1+NORDR1
24 CPV=CPV*Z+AZ(NORDR1-I+1+NSTART)
      RETURN
END
```

## REFERENCES

- [1]. Huang, T.S., "Stability of two-dimensional recursive filters," IEEE Trans. on Audio and Electroacoustics, Vol. AU-20, No. 2, June 1972.
- [2]. Shanks, J.L., TREITEL, S., and Justice, J.H., "Stability and synthesis of two-dimensional recursive filters," IEEE Trans. on Audio and Electroacoustics, Vol. AU-20, No. 2, June 1972.
- [3]. Shanks, J.L., "Two-dimensional recursive filters," in 1969 SWIEECO Rec., pp. 19E1 - 19E8.
- [4]. Sandberg, I.W., "Floating-point-roundoff accumulation in digital filter realizations," Bell Syst. Tech. J., Vol. 46, Oct. 1967, pp. 1775-1791.
- [5]. Ni, M.D. and Aggarwal, J.K., "Two-dimensional digital filtering and its error analysis," IEEE Trans. on Computers, Vol. C-23, No. 9, September 1974.
- [6]. Kan, E.P.F. and Aggarwal, J.K., "Error analysis of digital filter employing floating-point arithmetic," IEEE Trans. Circuit Theory, Vol. CT-18, No. 6, November 1971.
- [7]. Kan, E.P.F. and Aggarwal, J.K., "Correction to 'Error analysis of digital filters employing floating-point arithmetic,'" IEEE Trans. Circuit Theory, Vol. CT-20, No. 3, September 1973.
- [8]. Liu, B., "Effect of finite word length on the accuracy of digital filters - A review," IEEE Trans. Circuit Theory, Vol. CT-18, No. 6, November 1971.
- [9]. Liu, B. and Kaneko, T., "Error analysis of digital filters realized with floating-point arithmetic," Proc. IEEE, Vol. 57, Oct. 1969, pp. 1735-1747.
- [10]. Thajchayapong, P. and Rayner, P.J.W., "Recursive digital filter design by linear programming," IEEE Trans. Audio and Electroacoustics, Vol. AU-21, No. 2, April 1973.
- [11]. Gold, B. and Rader, C.M., Digital Processing of Signals, New York: McGraw-Hill, 1969.
- [12]. Jury, E.I., Theory and Application of the z-Transformation method, John Wiley & Sons, Inc., New York, 1964.

- [13]. Oppenheim, A. V. and Weinstein, C. J., "Effects of finite register length in digital filtering and the fast Fourier transform", Proc. of IEEE, Vol. 60, No. 8, August 1972.
- [14]. Oppenheim, A. V. and Weinstein, C. J., "A comparison of round-off noise in floating point and fixed point digital filter realization", Proc. IEEE, Vol. 57, pp. 1181-1183, June 1969.
- [15]. Jackson, L. B., Kaiser, J. F., and McDonald, H. S., "An approach to the implementation of digital filters", IEEE Trans. on Audio and Electro-acoustics, Vol. AU-16, pp. 413-421, September 1968.
- [16]. Jackson, L. B., "On the interaction of roundoff noise and dynamic range in digital filters", Bell Systems Technical Journal, Vol. 49, pp. 159-184, February 1970.
- [17]. Jackson, L. B., "Roundoff-noise analysis for fixed-point digital filters realized in cascade or parallel form", IEEE Trans. Audio Electro-acoustics, Vol. AU-18, pp. 107-122, June 1970.
- [18]. Jackson, L. B., "An analysis of limit cycles due to multiplication rounding in recursive digital (sub) filters", Proc. 7th Annual Allerton Conf. Circuit System Theory, pp. 69-78, 1969.
- [19]. Ebert, P. M., Mazo, J. E., Taylor, M. G., "Overflow oscillations in digital filters", Bell System Journal, Vol. 48, pp. 2999-3020, November 1969.
- [20]. Rader, C. M. and Gold, B., "Effects of parameter quantization on the poles of a digital filter", Proc. IEEE, Vol. 55, pp. 688-689, May 1967.
- [21]. Farmer, C. H., and Gooden, D. S., "Rotation and stability of a recursive digital filter", Proc. of Two Dimensional Digital Signal Processing Conference, October 1971, Columbia, Missouri.
- [22]. Hall, E. L., "Comparison of computations for spatial frequency filtering", Proc. IEEE, Vol. 60, No. 7, pp. 887-891, July 1972.
- [23]. Hunt, B. R., "Computational considerations in digital image enhancement", Proc. of Two Dimensional Digital Signal Processing Conf., October 1971, Columbia, Missouri.
- [24]. Hall, E. L. and Kahveci, A., "High resolution image enhancement techniques", Proc. of Two Dimensional Digital Signal Processing Conf., October 1971, Columbia, Missouri.

- [25]. Bednar, J. B. and Farmer, C., "Stability of spatial digital filters", Mathematical Biosciences, Vol. 14, pp. 113-119, 1972.
- [26]. Aggarwal, J. K., "Input quantization and arithmetic roundoff in digital filters - A review", Network and Signal Theory, Peter Peregrinus Ltd., pp. 315-343, September 1972.
- [27]. Jackson, L. B., Kaiser, J. F., and McDonald, H. S., "An approach to the implementation of digital filters", IEEE Trans. on Audio and Electroacoustics, Vol. AU-16, pp. 413-421, September 1968.
- [28]. Kaplan, W., "Introduction to Analytic Functions", Addison-Wesley Publishing Company, Chapter 9, p. 165, 1966.
- [29]. Kuo, B. C., "Discrete-Data Control Systems", Prentice-Hall, Chapter 3, p. 53, 1970.

DISTRIBUTION LIST\*

Current AFOSR Contract F4460-71-C-0091

Joint Services Electronics Program Distribution List dated 18 August 1975

DEPARTMENT OF DEFENSE

Chief, R & D Division (340)  
Defense Communications Agency  
Washington, D. C. 20301

Defense Documentation Center (12)  
ATTN: DDC-TCA (Mrs. V. Caponio)  
Cameron Station  
Alexandria, Virginia 22314

Dr. A. D. Schnitzler  
Institute for Defense Analyses  
Science and Technology Division  
400 Army-Navy Drive  
Arlington, Virginia 22202

Dr. George H. Hellmeyer  
Office of Director of Defense  
Research and Engineering  
The Pentagon  
Washington, D. C. 20315

Director, National Security Agency  
Fort George G. Meade, Maryland 20755  
ATTN: Dr. T. J. Beahn

DEPARTMENT OF THE AIR FORCE

HQ/USAF (AF/RDPE)  
Washington, D. C. 20330

HQ USAF/RDPB  
Washington, D. C. 20330

Rome Air Development Center  
ATTN: Documents Library (TILD)  
Griffiss AFB, New York 13440

Mr. M. E. Webb, Jr. (DCP)  
Rome Air Development Center  
Griffiss AFB, New York 13440

AFSC (CC)/Mr. Irving R. Mirman  
Andrews AFB  
Washington, D. C. 20334

Directorate of Electronics & Weapons  
HQ AFSC/DLC  
Andrews AFB, Maryland 20334

Directorate of Science  
HQ/APSC/DLS  
Andrews AFB, Washington, D. C. 20331

Mr. Carl Sletten  
AFCLR/LZ  
L. G. Hanscom Fld, Bedford, MA 01730

Dr. Richard Picard  
AFCLR/OP  
L. G. Hanscom Fld, Bedford, MA 01730

LTC J. W. Gregory (5)  
AF Member, TAC  
Air Force Office of Scientific Research  
1400 Wilson Blvd.  
Arlington, Virginia 22209

Mr. Robert Barrett  
AFCLR/LQ  
L. G. Hanscom Fld, Bedford, MA 01730

Dr. John N. Howard  
AFCR/CA  
L. G. Hanscom Field  
Bedford, Massachusetts 01730

HQ ESD (DRI/Stop 22)  
L. G. Hanscom Field  
Bedford, Massachusetts 01730

Professor R. E. Fontana  
Head Dept of Electrical Engineering  
AF IT/ENF  
Wright-Patterson AFB, Ohio 45433

AFAL/TE, Dr. W. C. Eppers, Jr.  
Chief, Electronics Technology Division  
Air Force Avionics Laboratory  
Wright-Patterson AFB, Ohio 45433

AF Avionics Lab/CA  
ATTN: Dr. Robert J. Doran  
Acting Chief Scientist  
AF Avionics Laboratory  
Wright-Patterson AFB Ohio 45433

AFAL/TEA (Mr. R. D. Larson)  
Wright-Patterson AFB, Ohio 45433

Faculty Secretariat (DFSS)  
US Air Force Academy  
Colorado 80840

Howard H. Steenbergen  
Chief, Microelectronics Development  
& Utilization Group/TE  
Air Force Avionics Laboratory  
Wright-Patterson AFB, Ohio 45433

Dr. Richard B. Mack  
Physicist  
Radiation and Reflection Branch (LZR)  
Air Force Cambridge Research Laboratories  
L. G. Hanscom Field, Bedford, MA 01730

Charles S. Sahagian  
Chief, Preparation and Growth Branch (LO)  
Air Force Cambridge Laboratories  
L. G. Hanscom Field, Bedford, MA 01730

Major William Peterson  
Assistant Chief, Information Processing Branch (ISI)  
Rome Air Development Center  
Griffiss AFB, NY 13441

LTC Richard J. Gowen  
Professor and Deputy Department Head  
Dept. of Electrical Engineering  
USAF Academy, Colorado 80840

Director, USAF Project RAND  
Via: Air Force Liaison Office  
The RAND Corporation  
ATTN: Library D  
1700 Main Street  
Santa Monica, California 90406

AUL/LSE-9663  
Maxwell AFB, Alabama 36112

AFETR Technical Library  
P. O. Box 4608, MU 5650  
Patrick AFB, Florida 32925

ADTC (SSLT)  
Eglin AFB, Florida 32542

HQ AMD (RDR/Col Godden)  
Brooks AFB, Texas 78235

USAFSAM (RAT)  
Brooks AFB, Texas 78235

Commander (2)  
ATTN: STEWB-AD-L, Technical Library  
White Sands Missile Range, New Mexico 88002

USAF European Office of Aerospace Research  
Technical Information Office  
Box 14, FPO New York 09510

VELA Seismological Center  
312 Montgomery Street  
Alexandria, Virginia 22314

Dr. Carl E. Baum  
AFWL (EE)  
Kirtland AFB, New Mexico 87117

Hqs Elect Sys Division (APBC)  
ATTN: ESD/MCIT/Stop 36  
Mr. John Mott/Smith  
Laurence G. Hanscom Field,  
Bedford, Mass 01730

USAFSAM/RAL  
Brooks AFB, Texas 78235  
Paul M. Keleghan, Supervisor  
Prog. Div., Geophy. Dept.  
Smithsonian Institution  
60 Garden Street  
Cambridge, Mass. 02138

DEPARTMENT OF THE ARMY

HODA (DARD-ARS-P)  
Washington, DC 20310

Commander  
US Army Security Agency  
ATTN: IARD-T  
Arlington Hall Station  
Arlington, Virginia 22212

HO Army Material Command  
Technical Library Rm 78 35  
5001 Eisenhower Avenue  
Alexandria, Virginia 22304

Commander (AMORD-BAD)  
US Army Ballistics Research Laboratory  
Aberdeen Proving Ground  
Aberdeen, Maryland 21005

Commander  
Picatinny Arsenal  
Dover, NJ 07701  
ATTN: Science & Tech Info Br  
SMUPA-TS-T-8

Dr. Hermann Robl  
US Army Research Office  
P. O. Box 12211  
Research Triangle Park  
North Carolina 27709

Richard O. Ulsh (CRDARD-IP)  
US Army Research Office  
P. O. Box 12211  
Research Triangle Park  
North Carolina 27709

Mr. George C. White, Jr.  
Deputy Director, L1000, 64-4  
Pitman-Dunn Laboratory  
Frankford Arsenal  
Philadelphia, Pennsylvania 19137

Redstone Scientific Information Center  
ATTN: Chief, Document Section  
US Army Missile Command  
Redstone Arsenal, Alabama 35809

Commander  
US Army Missile Command  
ATTN: AMBMBI-RR  
Redstone Arsenal, Alabama 35809

COL Robert W. Noce  
Senior Standardization Representative  
US Army Standardization Group, Canada  
Canadian Forces Headquarters  
Ontario, Ontario, Canada K1A 0K2

Dr. Homer F. Priest  
Chief, Materials Sciences Division, Bldg. 292  
Army Materials and Mechanics Research Center  
Watertown, Massachusetts 02172

John E. Rosenberg  
Harry Diamond Laboratories  
Connecticut Ave & Van Ness Street N. W.  
Washington, DC 20438

Commandant  
US Army Air Defense School  
ATTN: ATBASD-T-CSM  
Fort Bliss, Texas 79916

\*The Joint Services Technical Advisory Committee has established this list for the regular distribution of reports on the electronics research program of the University of Texas at Austin. Additional addresses may be included on their written request to:

Mr. I. A. Belton (AMSEL-TL-DC)  
Executive Secretary, TAC/JSEP  
US Army Electronics Command

Fort Monmouth, New Jersey 07703

As appropriate endorsement by a Department of Defense sponsor is required except on request from a Federal Agency.

**Commandant**

US Army Command and General Staff College  
ATTN: Acquisitions, Lib Div  
Fort Leavenworth, Kansas 66027

Dr. Hans K. Ziegler (AMSEL-TL-D)

Army Member, TAC/JSEP

US Army Electronics Command

Fort Monmouth, New Jersey 07703

Mr. I. A. Balton, (AMSEL-TL-DC) (S)

Executive Secretary, TAC/JSEP

US Army Electronics Command

Fort Monmouth, New Jersey 07703

Mr. A. D. Bedrosian, Rm 26-131

US Army Scientific Liaison Office

Mass Institute of Technology

77 Massachusetts Avenue

Cambridge, Massachusetts 02139

Director (NV-D)

Night Vision Laboratory, USAECOM

Fort Belvoir, Virginia 22060

Commander/Director

Atmospheric Sciences Laboratory

ATTN: AMSEL-EL-DD

White Sands Missile Range, New Mexico 88002

Atmospheric Sciences Laboratory

US Army Electronics Command

ATTN: AMSEL-EL-RA (Dr. Holt)

White Sands Missile Range, New Mexico 88002

Chief, Missile EW Tech Area

Electronic Warfare Laboratory, ECOM

ATTN: AMSEL-WL-MY

White Sands Missile Range, New Mexico 88002

US Army Armaments

ATTN: AMSAM-RD

Rock Island, Illinois 61201

US Army ABMDA

(ATTN: RDMD-NC, Mr. Gold)

1300 Wilson Blvd.

Arlington, VA 22208

Harry C. Holloway, M. D. Col., MC

Director, DIV of Neuropsychiatry

Walter Reed Army Institute of Research

Washington, DC 20012

Commander, USABATCOM

AMCPM-SC

Fort Monmouth, New Jersey 07703

Director, TRI-TAC

ATTN: TT-AD (Mrs. Brillier)

Fort Monmouth, N. J. 07708

Commander

US Army R & D Group (Far East)

APO, San Francisco, California 96343

Commander, US Army Communications Command

ATTN: Director, Advanced Concepts Office

Fort Huachuca, AZ 85613

Project Manager, ARTAD6

(AMCPM-TDS)

EAI Building

West Long Branch, NJ 07764

US Army White Sands Missile Range

STEWNS-ID-R (ATTN: Dr. Alton L. Gilbert)

White Sands Missile Range, NM 88008

Mr. William T. Kawai

US Army R & D Group (PAC EAST)

APO, San Francisco, California 96343

Commander

US Army Electronics Command

Fort Monmouth, New Jersey 07703

ATTN: AMSEL-RD-O (Dr. W. S. McAfee)

CT-L (Dr. G. Buser)

CT-LE (Dr. S. Epstein)

EL-FM-A

CT-D

CT-R

NL-O (Dr. H. S. Bennett)

NL-T (Dr. R. Kulinyi)

NL-C

NL-PB

NL-F

NL-M

TL-I

TL-B

VL-D

TL-MM (Mr. Lipetz)

EL-FM (Dr. Edward Collett)

NL-O

NL-X

NL-H Schuringa

NL-Y

TL-DR

TL-E (Dr. S. Kronenberg)

TL-E (Dr. J. Kohn)

TL-I (Dr. C. Thornton)

NL-B (Dr. S. Amoroso)

**DEPARTMENT OF THE NAVY**

Director, Electronic Programs

ATTN: Code 427

Office of Naval Research

800 North Quincy Street

Arlington, Virginia 22217

Director

Naval Research Laboratory

ATTN: Mr. A. Brodzinsky, Code 5200

Washington, DC 20390

Director

Naval Research Laboratory

ATTN: Library, Code 2629 (ONRL)

Washington, DC 20390

Dr. G. M. R. Winkler

Director, Time Service Division

US Naval Observatory

Washington, DC 20390

Naval Weapons Center

Technical Library (Code 753)

China Lake, California 93555

Director

Information Systems Program (437)

Office of Naval Research

Arlington, Virginia 22217

Director, Naval Research Lab (Code 6400)

4555 Overlook Avenue, S. W.

Washington, DC 20375

Director, Naval Research Laboratory (Code 5470)

4555 Overlook Avenue, S. W.

Washington, DC 20375

Dr. Leo Young (Code 5203)

Electronics Division

Naval Research Laboratory

Washington, DC 20375

Commander

Naval Training Equipment Center

Orlando, Florida 32813

Dr. A. L. Blaikie

Scientific Advisor, Code AX

Hqs. US Marine Corps

Washington, DC 20380

US Naval Weapons Laboratory

Dahlgren, Virginia 22448

Commander

US Naval Ordnance Laboratory

Silver Spring, Maryland 20910

ATTN: Tech Library & Info Services Div.

Director

Office of Naval Research

Boston Branch

495 Summer Street

Boston, Massachusetts 02210

Commander

Naval Missiles Center

ATTN: 5832.2, Technical Library

Point Mugu, California 93042

Commander

Naval Electronics Laboratory Center

ATTN: Library

San Diego, California 92152

Deputy Director and Chief Scientist

Office of Naval Research Branch Office

1030 East Green Street

Pasadena, California 91106

Superintendent

Naval Post Graduate School

Monterey, California 93940

ATTN: Library (Code 2124)

Officer in Charge, New London Lab

Naval Underwater Systems Center (TECB Library)

New London, Connecticut 06320

Commander

Naval Avionics Facility

ATTN: D/035 Technical Library

Indianapolis, Indiana 46241

Commander

Office of Naval Research Branch Office

535 South Clark Street

Chicago, Illinois 60605

Naval Air Development Center

ATTN: Technical Library

Johnsville

Warminster, Pennsylvania 18974

Naval Oceanographic Office

Technical Library (Code 1640)

Suitland, Maryland 20330

Naval Ship Research and Development Center

Central Library (Code 142 and 143)

Washington, DC 20007

**OTHER GOVERNMENT AGENCIES**

Mr. F. C. Schwenk, RD-T

National Aeronautics & Space Administration

Washington, DC 20546

Los Alamos Scientific Laboratory

ATTN: Reports Library

P O Box 1663

Los Alamos, New Mexico 87544

M. Zene Thornton

Deputy Director Institute for Computer

Sciences & Technology

National Bureau of Standards

Washington, DC 20234

Director, Office of Postal Technology (R&D)

US Postal Service

1717 Parklawn Drive

Rockville, Maryland 20852

NASA Lewis Research Center

ATTN: Library

2100 Brookpark Road

Cleveland, Ohio 44135

Library -R51

Bureau of Standards

Acquisition

Boulder, Colorado 80302

MIT Lincoln Laboratory

ATTN: Library A-082

P. O. Box 73

Lexington, Massachusetts 02173

Dr. Jay Harris

Program Director, Devices and Waves Program

NSF

1800 G Street

Washington, DC 20550

Dr. Howard W. Etzel

Deputy Director, Div. of Materials Resch

NSF

1800 G Street

Washington, DC 20550

Dr. Dean Mitchell

Program Director, Solid-State Physics

Division of Materials Research

National Science Foundation

1800 G Street

Washington, DC 20550

**NON-GOVERNMENT AGENCIES**

Director

Research Laboratory of Electronics

Massachusetts Institute of Technology

Cambridge, Massachusetts 02139

Director

Microwave Research Institute

Polytechnic Institute of New York

Long Island Graduate Center, Route 110

Farmingdale, New York 11735

Mr. Jerome Fox, Research Coordinator

Polytechnic Institute of New York

333 Jay Street

Brooklyn, New York 11201

Director

Columbia Radiation Laboratory

Dept. of Physics

Columbia University

535 West 120th Street

New York, New York 10027

Director

Coordinated Science Laboratory

University of Illinois

Urbana, Illinois 61801

Director

Stanford Electronics Laboratory

Stanford University

Stanford, California 94305

Director

Microwave Laboratory

Stanford University

Stanford, California 94305

Director

Electronics Research Laboratory

University of California

Berkeley, California 94720

Director

Electronics Sciences Laboratory

University of Southern California

Los Angeles, California 90007

Director

Electrophysics Research Center

The University of Texas at Austin

Engineering-Science Bldg. 112

Austin, Texas 78712

Director of Laboratories

Division of Engineering & Applied Physics

Harvard University

Pierce Hall

Cambridge, Massachusetts 02138